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Gravitational wave generator apparatus

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Abstract

An apparatus or structure is proposed for generating high-frequency gravitational waves (HFGWs) between pairs of force-producing elements by means of the simultaneous production of a third time derivative of mass motion of the pair of force-producing elements. The elements are configured as a cylindrical array in the proposed structure and are activated by a radiation wavefront moving along the axis of symmetry of the array. The force-producing elements can be micro-electromechanical systems or MEMS resonators such as film-bulk acoustic resonators or FBARs. A preferred cylindrical array is in the form of a double helix and the activating radiation can be electromagnetic as generated by microwave transmitters such as Magnetrons. As the activating radiation wavefront moves along the axis of the structure it simultaneously activates force elements on opposite sides of the structure and thereby generates a gravitational wave between the pair of force elements. It is also indicated that the Earth is completely transparent to the HFGWs. Thus a sensitive HFGW detector, such as the Li-Baker under development by the Chinese, can sense the generated HFGW at an Earth-diameter distance and could, in theory, be a means for implementing transglobal HFGW communications.

Keywords: Gravitational waves, high-frequency gravitational wave generator, HFGW, communication, MEMS, FBARS

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Introduction

As will be discussed there exist several sources for high-frequency gravitational waves (HFGWs) or means for their generation. Historically the first generation means, which is the same for gravitational waves (GWs) of all frequencies, is based upon the quadrupole equation first derived by Einstein 1918 [1]. A formulation of the quadrupole (Baker, 2006) that is easily related to the orbital motion of binary stars or black holes, rotating rods, laboratory HFGW generation, etc. is based upon the jerk or shake of mass (time rate of As will be discussed there exist several sources for high-frequency gravitational waves (HFGWs) or means for their generation. Historically the first generation means, which is the same for gravitational waves (GWs) of all frequencies, is based upon the quadrupole equation first derived by Einstein 1918 [1]. A formulation of the quadrupole (Baker, 2006) that is easily

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related to the orbital motion of binary stars or black holes, change of acceleration), such as the change in centrifugal force vector with time; for example as masses move around each other on a circular orbit. Figure 1 describes that situation. Recognize, however, that change in force Δf need NOT be a gravitational force (see Einstein; Infeld quoted by Weber [2]. Grishchuk and Sazhin [3]). Electromagnetic forces are more than 10^{35} times larger than gravitational forces and should be employed in laboratory GW generation. As Weber [2] points out: ÈThe non-gravitational forces play a decisive role in methods for detection and generation of gravitational waves ...Š The quadrupole equation is also termed Èquadrupole formalismŠ and holds in weak gravitational fields (but well over 100 gÑs), for speeds of the generator ÈcomponentsŠ less than the speed of light and for the distance between two masses *r* less than the GW wavelength. Certainly there would be GW generated for *r* greater than the GW wavelength, but the quadrupole ÈformalismŠ or equation might not apply exactly. For very small time change Δt the GW wavelength, $\lambda_{GW} = c\,\Delta t$ (where c ~ 3×10^8 m s^{-1}, the speed of light) is very small and the GW frequency ν_{GW} is high. The concept is to produce two equal and opposite jerks or Δf õs at two masses, such as are involved in micro-electromechanical systems (MEMS), for example film-bulk acoustic resonators (FBARs), a distance 2*r* apart. This situation is completely analogous to binary stars on orbit as shown in Fig. 1.

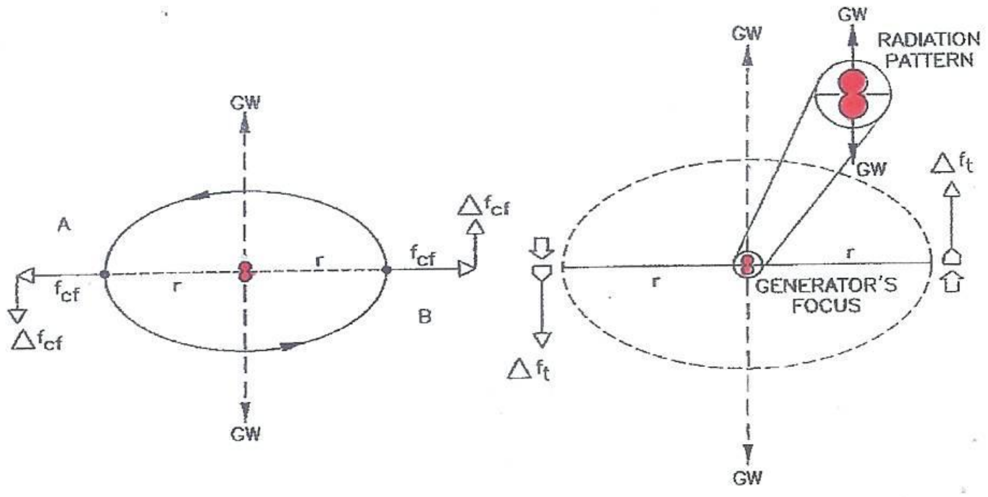


Fig. 1. Change in centrifugal force of orbiting masses, Δf_{cf}, that produces GW radiation

2. Discussion

Next we consider an array of GW sources. Consider a stack of binary star orbit planes, each one involving a pair of masses circling each other on opposite sides of a circular orbit as shown in Fig. 3. Let the planes be stacked one light hour apart (that is, $60 \times 60 \times 3 \times 10^8 = 1.08\times10^{12}$ meters apart) and each orbit exactly on top of another (coaxial circles). Let us also suppose that the periods of the orbits were 10 hours. The orbital ÈfrequencyŠ would then be $1/10\times60\times60 = 2.8\times10^{-5}$ Hz. According Landau and Lifshitz [4] on each plane a GW will be generated that radiates from the center of each circular orbit. The details of that generation process are that as the masses orbit a radiation pattern is generated. In simplified terms (from the equations shown in an exercise on page 356 of Landau and Lifshitz, [4]) an elliptically shaped polarized arc of radiation is formed on each side of the orbit plane (mirror images). As the two masses orbit each other 180^0 the arcs sweep out a figure of revolution and the resulting integrated GW radiation is circularly polarized. Together these figures of revolution become shaped like a peanut as shown in Fig. 2. This situation occurs when the orbiting masses move half an orbital period 180^0 or 5 hours on their orbit. Thus the frequency of the GW generated is twice the orbital frequency or 5.6×10^{-5} Hz.

The general concept of the present HFGW generator is to utilize an array of force-producing elements arranged in pairs in a cylindrical formation. They could be piezo-rods connecting the two masses or individual resonators .In any event they would be analogous to the binary arrays of Fig. 3 in which an imaginary cylinder could be formed or constructed from the collection of circular orbits. As a wavefront of energizing radiation proceeds along the cylindrical axis of symmetry of such a cylindrical array, the force-producing element pairs (such as pairs of FBARs) are energized simultaneously and jerk, that is they exhibit a third time derivative of mass motion, in concert. The jerking generates gravitational waves focused midway between the jerking pairs exactly analogous to centrifugal force jerks of the orbiting binaries

2.1 Double helix

A convenient cylindrical array is a double helix exhibited in Fig. 4. In this case the MEMS or FBARs are placed along the opposing ribbons of the helixes. As activating radiation (e.g., magnetron-generated microwaves) moves along the axis of symmetry of the helixes, the opposing FBARs are energized and jerk thereby producing a HFGW. It is important that the activating radiation be phase-coherent. In order to understand this concept better let us return to the orbit-plane stack of Fig. 3. A GW generated by the first binary (at the base of the stack) should reach the second member of the stack at its center just as the GW arc is formed with the correct polarization and phase to match the upcoming GW. We imagined the polarization plane as the plane of an elliptical arc. Since the orbit planes are one light hour apart the orbiting binaries must be synchronized one hour of motion further along on their orbit from the initial locations, when they were exactly aligned, in order to reinforce the GW moving along the axis of the imaginary orbit-plane cylinder. Analogously the activating radiation of the double-helix cylindrical array must energize each FBAR pair as the GW passes. Thus if the energizing radiation is produced by microwave transmitters along the GW path (axis of symmetry of the helixes) they must be phase coherent. As will be discussed in more detail in the next following sub-section 2.2, the phase coherent HFGW flux or signal increases in proportion to the **square** of the number of MEMS (e.g., FBARs) HFGW-generation elements, *N* according to Dicke [5] and Scully and Svidzinsky [6].

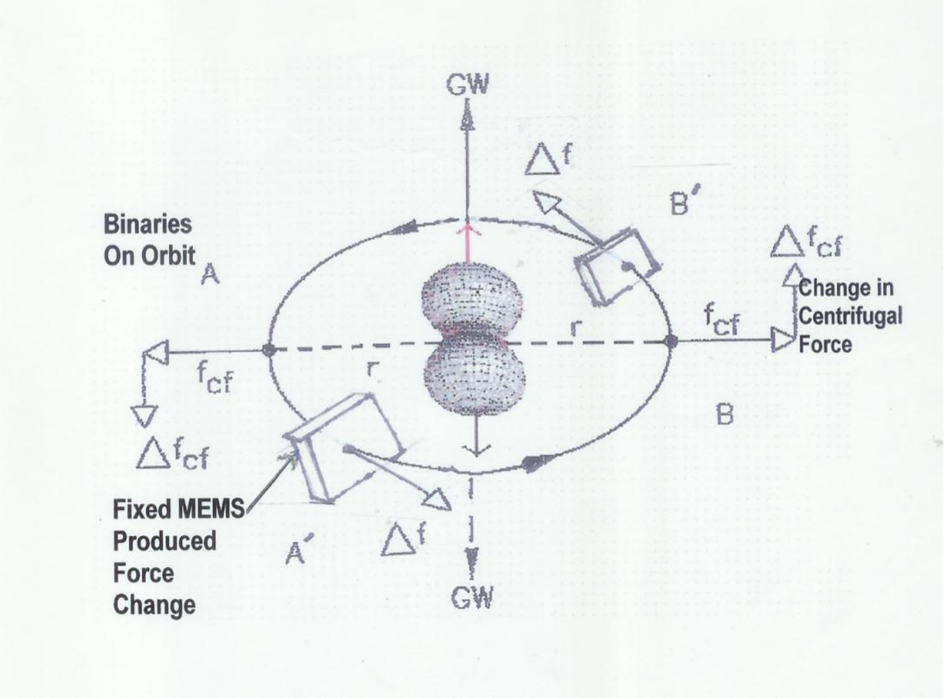
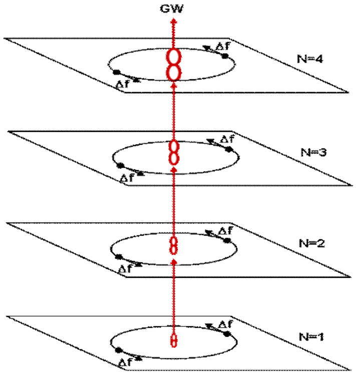


Fig. 2. Radiation pattern calculated by Landau and Lifshitz [4] Section 110 Page 356



Fig, 3. GW flux growth analogous to stack of *N* orbital planes

2.2 Superradiance

The N^2 build up, termed ÈSuperradiance,Š is attributed to two effects: one *N* from there being *N* HFGW power sources or generation elements and the other *N* from the narrowing of the beam so that the HFGW is more concentrated and the flux (W m^{-2}) thereby increased. Utilizing General Relativity, Romero-Borja and Dehnen and Dehnen and Romero-Borja [7], computed a superradiance build up of Èý needle-like radiation ý Š HFGWs beam from a closely packed but very long linear array of crystal oscillators. Their oscillators were essentially two vibrating masses that were a distance *b* apart whereas a pair of vibrating FBAR masses is a distance 2*r* apart as shown in Fig. 5. However, the FBAR operates in an analogous fashion as piezoelectric crystals. Superradiance also occurs when emitting sources such as atoms Èý are close together compared to the wavelength of the radiation ý Š (Scully and Svidzinsky, p.1510 [6]). Note that it is **not** necessary to have the MEMS or FBAR elements perfectly aligned (that is, the FBARs *exactly* across from each other) since it is only necessary that the energizing wave front (from Magnetrons in the case of the MEMS or FBARs as in Baker, Woods and Li, [8[) reaches a couple of nearly opposite FBARs at the same time so that a coherent radiation source or focus is produced between the two FBARs. The energizing transmitters, such as Magnetrons, can be placed along the helixesÑarray axes between separate segments of the array or, more efficiently, at the base of the double helixes so that a superradiance microwave beam is projected up the axis of the helixes. The force change, Δf, produced by energizing one off-the-shelf FBAR is 2 N according to Woods and Baker [9].

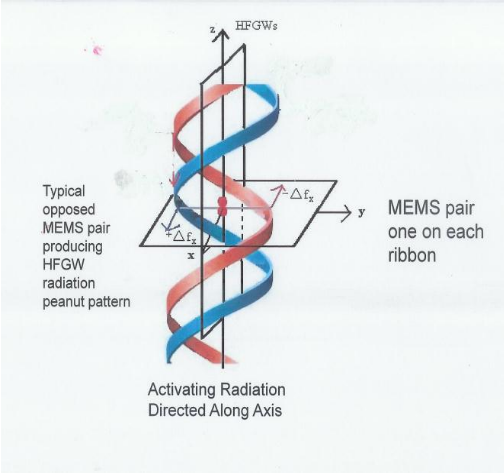


Fig. 4. Double-Helix HFGW generator FBAR array (Patent Pending).

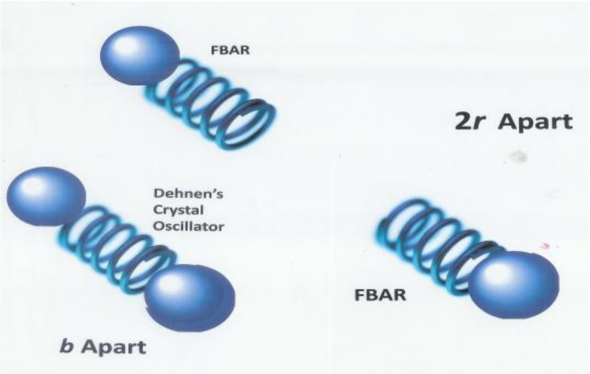


Fig. 5. Comparison of Dehnen and Romero-Borja [7] crystal oscillator and FBAR-pair system

2.3 Analogy and fabrication technique

In order to clarify the double-helix concept and its fabrication, let us consider a totally different yet analogous situation. It is a storage facility for mattresses. Each mattress is, say, 7 feet by 6 feet and one foot thick (analogous to a **gigantic MEMS or FBAR**). The storage-facility is composed of many coaxial cylindrical structures that are analogous to the cylindrical array of MEMS. The cylindrical structures consist of 7-foot wide compartments between the cylindersÑinside and outside walls and each of these compartments are 6-feet high. Thus one can store one mattress on its side in each compartment. In order to reach a given compartment, imagine that two escalators are installed on the inside wall of each cylindrical structure. They are in the form of spiral escalators ÈstairwaysŠ and are constructed on exactly opposite sides of each cylindrical storage structure (essentially the ribbons of a **double helix** of MEMS). As an example, let us consider one of the cylindrical structures that happen to have a diameter of 100 feet. The circumference of the inside wall of the cylinder is about 314 feet so that the foot of the opposite escalator is about 157 feet distant from its opposite. We take the tread of each escalator step as one foot wide (enough room to slide a mattress in or out of its compartment when the escalator is periodically halted). We want to be able to reach each mattress so the escalators must rise 6 feet in 157 feet in the first 6-foot- high floor of the storage structure. Thus the height of each escalator step when it is moving is 6/157 of a foot or about 1/32 of an inch. Two people start up on each escalator simultaneously, which is analogous to a **wavefront from a Magnetron** moving up a double helix of FBARs. They proceed up from compartment to compartment. At each of the 157 ÈlevelsŠ **(*N*)** they reach opposite pairs of mattresses. In the analogous manner the wave front reaches opposite FBARs and excites them and produces a jerk and, therefore, HFGW radiation pattern focused between the FBARs. But what about the other coaxial cylindrical mattress storage cylinder structures? In order to transport the mattresses the tread width needs to be kept constant that is, more levels on cylinder structures having inside diameters of more than 100 feet and fewer levels on cylinder structures having diameters less than 100 feet. Thus each level is distinct and every mattress pair is on a uniquely different level (there are *N* such different levels and, hence, mattress pairs). Also the escalators for each cylinder could be located at different starting points on the circumference of a given cylinder structure. For example, if there were ten structures, then one could place them on different azimuths such as 0, 18, 36, 54, 72, 90, 108, 126, 144 and 162 degrees or at random. Such options may be considered in the fabrication or building process of the imaginary mattressµstorage cylindersÑconstruction or, analogously, **the FBAR array fabrication**. In order to develop the double helix winding, a column could be fabricated with the mattress joined that is, glue the mattresses back to back one mattress to the next in a long line. This would create a 6-foot by 7µfoot cross-section tube or, for the analogous FBARs, a 110 µm by 110 µm thread (or whatever the dimensions of the trimmed FBAR MEMS are). Then place one tube on top of the other after 157 feet. Thus the composite tube exhibits a 7-foot by 2×6 = 12-foot rectangular cross-section. The analogous FBAR construction would be a 110 µm by 220 µm rectangular cross-section thread. The FBAR fabrication would continue by tightly-winding the composite threads around a microwave-transparent cylinder or spool, layer after layer in order to form the ribbons of the double helix. Thus **the resulting double-helix structure** could be inserted in the microwave guide. Returning to the mattress analogy, it is recognized that each escalator passenger may take off at slightly different time, analogous to slightly **irregular**

wave front. They all, however, will ascend at the same speed: the speed of light in the structure. Such wavefront irregularities would however be mitigated or eliminated by a properly designed waveguide.

3. Results

As a numerical example or result of a double-helix FBAR array analysis, we will choose the median radius of the overall array as r = 20 cm (convenient laboratory size though usually somewhat greater than λ_{GW}), Δf = 2 N for an off-the-shelf FBAR and $\Delta t = 4\times10^{-10}$ s (equivalent to about a ν_{EM} = 2.5 GHz frequency or pulse of the jerk or energizing radiation frequency) so that λ_{EM} =12 cm and λ_{GW} = 6 cm (the frequency of the GW is twice that of the frequency of the energizing EM wave) and the power, *P* from the basic GW equation (its derivation can be found in, for example, Baker [10]. found by hyperlink at http://www.gravwave.com/docs/Astronomische%20Nachrichten%202006.pdf))

$$P=1.76\times10^{-52}\,(2r\,\Delta f/\Delta t)^2 \text{ W}. \qquad (1)$$

For this equation the calculation of the combined ¦ f of all the pulsating MEMS or FBARs requires more calculation. We will set the length of a double-helix array cylinder as 20 m, but recognize that it can be separated into segments along the same axis with energizing transmitters, e.g., Magnetrons installed on the cylinder axis between the segments. As previously mentioned the transmitters could also be phase coherent and arranged in a line along the double-helix axis at its base. If, for example, there were 1000 one-kilowatt Magnetrons (such as those installed in a conventional microwave oven and feeding in on one hundred 12-cm, λ_{EM}, wide levels) and each of their beams covered a 10-cm radius circle, then the energizing radiation flux would be 3.2×10^4 W m^{-2}. According to superradiance there would result a needle-like microwave radiation directed along the axis of the double helixes amounting to 32 gigawatts per square meter. In order to create a perfectly planner wave front, with no irregularities, the cylindrically symmetric MEMS array would be contained in a waveguide or possibly a very wide coaxial Ècable,Š surrounded by a robust one-megawatt heat sink. To increase instantaneous power to the array, bursts of gigawatt power, for example, every millisecond could be employed that would maintain a megawatt average power input. The walls of the cylindrical array are taken to be 30 cm thick. Thus the volume of the array is $\pi(r_1^2\ \mu\ r_2^2)\times20$ m^3, where r_1 is the outside radius = 0.35 m and r_2 is the inside radius = 0.05 m. Thus the volume is 7.5 m^3. A FBAR (Fig. 6) is a mechanical (acoustic) resonator consisting of a vibrating membrane (typically about 100×100μm^2 in plan form, and about 1μm thickness), fabricated using well-established integrated circuit (IC) micro fabrication technology. A typical off-the-shelf FBAR as shown schematically in Fig. 6, usually has overall dimensions 500 μm by 500 μm by approximately 100 μm thick. For our purposes, in which a high number density is important, we will trim the FBARs to a minimum size. In order to account for fabrication margins we will take the dimensions as 110 μm by 110 μm by 20 μm for an FBAR volume of $2.42\times10^{-13}m^3$. However, it could be smaller as shown in Fig.1 of Chan, et al. [11] (the MEMS resonator shown there is about 50 μm square by 2 μm thick for a volume of about 10^{-14} m^3).

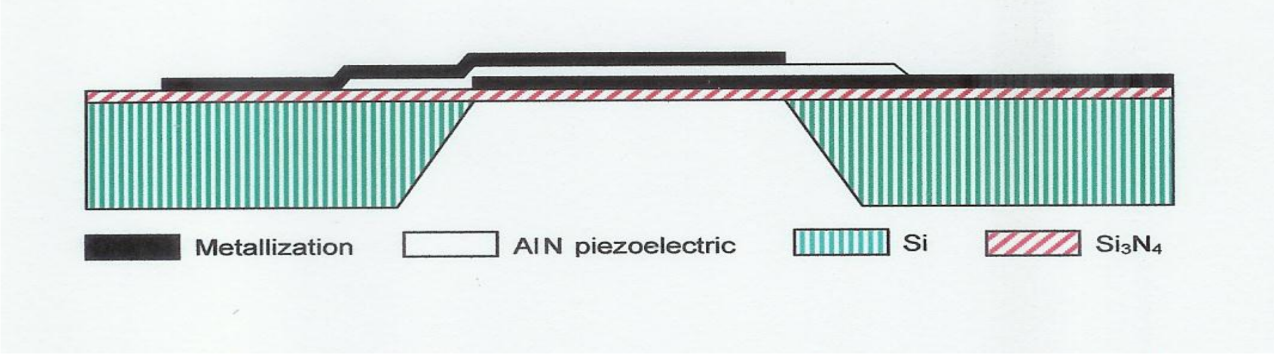


Fig. 6. Basic FBAR construction (cross-section side view, not to scale)\

Thus the total number of FBARs in the double-helix cylindrical array is 3. 1×10^{13} and the number of pairs is half of that. Thus there will be $N = 1.55\times10^{13}$ FBAR pairs in the double-helix cylindrical array. Since each FBAR exhibits a jerking force of 2 N the combined ¦ f of all the jerking FBAR pairs is 3.1×10^{13} N if the jerking pairs (or ÈorbitsŠ) were collapsed and moved in concert analogous to the orbit plane with the synchronized orbital mass motion.

3.1 Standard approach

As the energizing wave front moves up the axis of the double helix it develops the HFGW wave as if it were a single unified system with one ever accumulating, mass-change effect so that effectively the mass change ¦ f = 3.1×10^{13} N. Thus from Eq. (1), with $2r_{\mathrm{rms}}$ = 2Ð[($r_1^2 + r_2^2$)/2] = 0.5 m, the total power produced by the double-helix array is $P = 1.76\times10^{-52}(0.5\times3.1\times10^{13} /(4\times10^{-10}))^2 = 2.64\times10^{-7}$ W. But due to the N levels, each one of which represents an individual GW focus, there exists a ÈSuperradianceŠ condition in which the HFGW beam becomes very narrow as shown schematically in Fig. B of Scully and Svidzinsky [6]. Thus the HFGW flux, in W m^{-2}, becomes much larger at the cap of the peanut shaped radiation pattern. According to the analyses of Baker and Black [12] the area of the *half-power cap* is given by:

$$A_{\mathrm{cap}} = A_{1/2(N=1)} / N \quad \mathrm{m}^2, \tag{2}$$

where $A_{1/2(N=1)} = 0.1358$ m^2 for a single level (N =1) at a distance of 0.282 m (radius of a one square meter area sphere) or $(1\mathrm{m}/0.282\mathrm{m})^2(0.1358) = 1.71$ m^2 at a distance of one meter. Thus Eq. (2) becomes $A_{\mathrm{cap}} = 1.71/N$ m^2 (actually one fourth of the HFGW power reaches the cap since half goes to the other side of the peanut-shaped radiation pattern in the µz direction in Figs. 2 and 3). Thus the HFGW flux at a one-meter distance from the end of the double-helix cylindrical array is:

$$S(1) = (P/4)/(1.71/N) = (2.64\times10^{-7} /4)/(1.71/1.55\times10^{13}) = 6 \times10^5 \mathrm{~W~m}^{-2} . \tag{3}$$

From Baker, et al. [13], Eq. (6A) of the Appendix, the amplitude of the dimensionless strain in the fabric of spacetime is:

$$A = 1.28\times10^{-18}\text{Ð}S/\nu_{GW} \text{ m/m.} \tag{4}$$

So that at a one-meter distance $A = 1.98\times10^{-25}$ m/m From Woods, et al., [14] the current **estimated sensitivity of the Chinese Li-Baker HFGW Detector is $A = 1.0\times10^{-30}$ m/m to 1.0×10^{-32} m/m** with a signal to noise ratio of over 1500 (Woods, et al, [14], p. 511) or if we were at a $1.3\mathrm{x}10^7$ m (diameter of Earth) distance, then $S = 3.55\times10^{-9}$ Wm^{-2} and the amplitude A of the HFGW is given by $A = 1.52\times10^{-32}$ m/m. There also could be a HFGW superconductor lens, as described by Woods [15] that could concentrate very high frequency gravitational waves at the detector or receiver. Thus with Chinese Li-Baker HFGW detector program successful and the WoodÑ lens practical, **the Li-Baker detector will exhibit sufficient sensitivity to receive the generated HFGW signal globally.**

3.2 Conservative approach

A more conservative approach would be that there are $N = 1.55\times10^{13}$ individual GW power sources each with a ¦ f = 2 N. Again from Eq. (1), with $2r_{\mathrm{rms}}$ = 2Ð[($r_1^2 + r_2^2$)/2] = 0.5 m, the total power produced by the double-helix array is $NP = 1.55\times10^{13} \times1.76\times10^{-52}(0.5\times2/4\times10^{-10})^2 = 1.7\times10^{-20}$ W. But, as already pointed out, due to the N levels, each one of which represents an individual GW focus, there exists a ÈSuperradianceŠ condition in which the HFGW beam becomes very narrow as shown schematically in Fig. B of Scully and Svidzinsky [6]. Thus the HFGW flux, in W m^{-2}, becomes much larger at the cap of the peanut shaped radiation pattern. Again according to Eq. (2) $A_{\mathrm{cap}} = 1.71/N$ m^2. Thus, according to Eq. (3) the HFGW flux at a one-meter distance from the end of the double-helix cylindrical array is: $S(1) = (NP/4)/(1.71/N) = (1.7\times10^{-20}/4)/(\ 1.71/1.55\times10^{13}) = 3.8\times10^{-8}$ W m^{-2} .. . From Eq. (4) at a one-meter distance $A = 5\times10^{-32}$ m/m. If the FBARs in all of the helix levels are not activated as individual pairs, then the situation changes. For example, let all of the FBARs in a 6-cm wide level (½ λ_{EM}) be energized in concert. The number of levels would be reduced to N = 20 m/0.06 m = 333. But, because the FBAR-pairs in each level act together, ¦ f = (2 N)(1.55×10^{13} / 333). Thus no matter how many activation divisions (N) the changes in Eq. (1) cancel out (the N^2) and there is no change in HFGW flux. If we were at a $1.3\text{x}10^7$ m (diameter of Earth) distance, then $S = 1.33\times10^{-20}$ Wm^{-2} and the amplitude A of the HFGW is given by $A = 3.8\times10^{-39}$ m/m. Although the best theoretical sensitivity of the Li-Baker HFGW detector is on the order of 10^{-32} m/m, its sensitivity can be increased dramatically [16] by introducing superconductor resonance chambers into the interaction volume (which also improves the Standard Quantum Limit; Stephenson [17] and two others between the interaction volume and the two microwave receivers. Together they provide an increase in sensitivity of five orders of magnitude and result in a theoretical sensitivity of the Li-Baker detector to HFGWs having amplitudes of 10^{-37} m/m. There also could be a HFGW superconductor lens, as described by Woods [15] that could concentrate very high frequency gravitational waves at the detector or receiver. Thus with Chinese Li-Baker HFGW detector program successful and the WoodÑ lens practical, so again the Li-Baker detector will exhibit sufficient sensitivity to receive the generated HFGW signal globally. The HFGW beam is very narrow. From Eq. (4b) of Baker and Black [12] for $N = 1.55\times10^{13}$ it would be $\sin^{-1}$ (0.737)/ Ð$1.55\times10^{13} = 1.87\times10^{-7}$ radians. For N = 333 the angle is 0.0022 radians. This is still narrow, but the double helix configuration certainly reduces the width of the HFGW beam. Additionally multiple HFGW carrier frequencies can be used, so the signal is very difficult to intercept, and is therefore useful as a low-probability-of-intercept (LPI) signal, even with widespread adoption of the HFGW

3.3 Irregularities

There are at least three irregularities that affect the performance of the double-helix generator design, especially in the standard approach. First is the ability to separate or differentiate the $N = 1.55\times10^{13}$ FBAR pairs due to irregularities in the fabrication of the helix ribbons. Second is the irregularity in the wave front of the energizing microwave radiation produced by the Magnetrons. Third are irregularities in the delay time between the incidence of the energizing or activating microwave radiation and the FBAR mechanical force change. At first glance the required positioning accuracy for MEMS, specifically FBARs, of 0.155 pedometers would seem to be impossible to achieve using conventional assembly techniques. On the other hand, the tight machine winding of the 110 μm by 220 μm rectangular cross-section FBAR threads in a dust-free environment, might have a tolerance of less than a small fraction of a nanometer. It is to be recognized that the simultaneous energizing of two FBARs produces GW radiation at the midpoint of a line exactly between them. If, for example, *every* ten FBAR pairs are slightly out of alignment and their lines intersect when energized, then the total power of the created GW would effectively be due to ¦ f = $2\text{N}\times1.55\times10^{13}\times10 = 3.1\times10^{14}$ N force change, but the number of such levels (of 10 common, undifferentiated FBAR pairs) would be N-10 = 1.55×10^{12} . The resulting beam would be much broader and hence the flux would be less. However the power at each GW generation site would be greater Thus the effect would not be as drastic as one might at first believe. Other scenarios could be imagined in which pairs of FBARs were simultaneously energized at sites not directly across from each other, but hopefully nanotechnology assembly techniques will obviate the problem. The irregularity in the wave front of the energizing microwave radiation produced but the Magnetrons is a more vexing design problem. If the irregularities in the wave front has cylindrical symmetry, then several superimposed GW beams will be generated in which the total power remains the same, but as in the prior situation, the beam is broadened and the HFGW flux reduced. Proper microwave- guide design of the manifold of multiple Magnetron radiation input will be essential in any event. There will be a delay between the incidence of the energizing or activating microwave radiation and the FBAR mechanical force change and if the delay is exactly the same for all FBARs, then there is no problem. If the delay has cylindrical symmetry about the axis of the helixes (e.g., due to some thermal effect) then the effect is as previously found, an increase in beam width and a resulting decrease in HFGW flux. Efforts will need to be made to manufacture and assemble the FBARs in a very uniform manner and to carefully control their environment after fabrication in the detector.

4. Conclusions

The overall concept is shown in Fig. 7 in very simplified form. In theory the preferred double-helix array of force-producing FBARs can generate significant superradiant HFGW radiation. A numerical example of a 20-meter long array is presented. Activation-energy radiators or transmitters (such as off-the-shelf Magnetrons) can be utilized to energize MEMS such as off-the-shelf FBARs found in cell phones. Thus point-to-point communication, even at a distance of the diameter of the Earth, might be realized using very sensitive HFGW Chinese detectors or receivers and HFGW lenses to concentrate the HFGW signal at the receivers

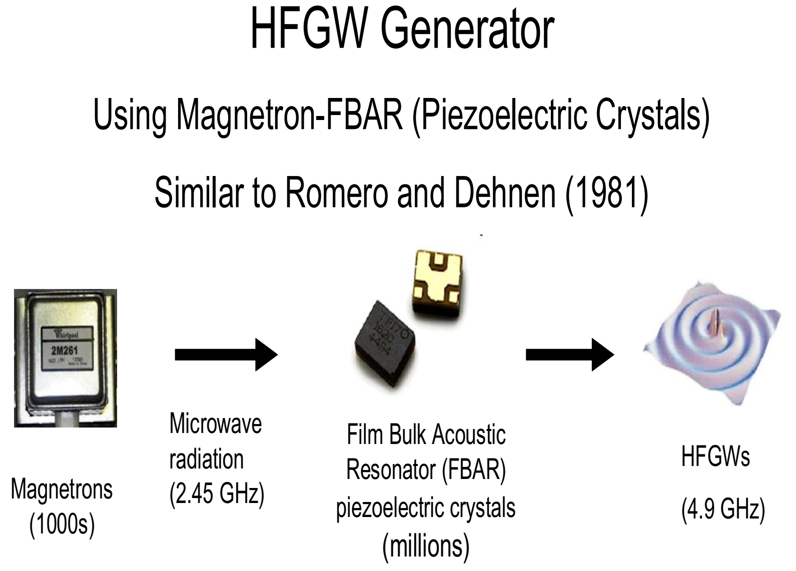


Fig. 7. Simplified concept of the HFGW generator.

A HFGW amplitude of the time-varying strain of the fabric of spacetime, $A = 3.8\times10^{-39}$ m/m is created at a distance of one Earth diameter from the generator. It is also indicated that the Earth is completely transparent to the HFGWs. Thus with a sensitive HFGW detector, such as the Li-Baker successfully developed by the Chinese and the WoodÑ lens practical, one could sense the generated HFGW at an Earth-diameter distance and could, in theory, be a means for transglobal communications.

The approach to the laboratory or manmade terrestrial generation of HFGWs is innovative and unique (Baker and Baker, [18]). There have been few other advances in the HFGW generation field. The General Relativity crystal oscillator studies by Romero-Borja and Dehnen (1981) and Dehnen and Romero-Borja (2003) [7], are probably the most important up to now, but its reliance on old-style crystals (not modern MEMS technology, discussed in Baker and Baker, [18]) and a linear rather than a cylindrically symmetric array resulted in a very inefficient HFGW generator. The methods discussed herein are the most appropriate to the science and engineering of terrestrial HFGW generation. All the relevant literature has been cited that supports the theory and fabrication of the proposed HFGW generator.

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