





## PAPER

## Quantum steering transfer within quantum network

Xiao-Gang Fan<sup>1,2</sup> , Jiaojiao Chen<sup>1</sup>, Wei Xiong<sup>3,4,\*</sup>, Dong Wang<sup>1</sup>  and Liu Ye<sup>1,\*</sup>

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<sup>1</sup> School of Physics and optoelectronics engineering, Anhui University, Hefei 230601, People's Republic of China<sup>2</sup> Key Laboratory of Functional Materials and Devices for Informatics of Anhui Educational Institutions, Fuyang Normal University, Fuyang, Anhui 236037, People's Republic of China<sup>3</sup> Department of Physics, Wenzhou University, Wenzhou 325035, People's Republic of China<sup>4</sup> International Quantum Academy, Shenzhen 518048, People's Republic of China

\* Authors to whom any correspondence should be addressed.

E-mail: [xiongweiphys@wzu.edu.cn](mailto:xiongweiphys@wzu.edu.cn) and [yeliu@ahu.edu.cn](mailto:yeliu@ahu.edu.cn)**Keywords:** quantum steering, adjustable measurements, quantum network**Abstract**

Quantum steering is the ability that one system affects another one without delay by performing local measurements, which has garnered significant attention in the field of quantum information science. Here, we propose a linear network to realize tunable quantum steering with adjustable measurements. We show that forward steering of the first entangled source can be perfectly transferred to the state of two endpoints, regardless of measurements in the quantum network. However, for the backward steering between two endpoints, it displays a four-leaf clovers with rich symmetries with measurement parameters  $\{\theta_j\}_{j=1}^{N-1}$  and is dependent on the parameters  $\{\beta_j\}_{j=2}^N$  of the input state. By tuning the measurements far away from or close to the optimal values, one-way or two-way steering can be controllably realized. In addition, the error between the actual and optimal measurements is also taken into account in our proposal. The result indicates that a smaller error is beneficial for predicting two-way steering involving multiple measurements. Our proposal offers a promising way to realize the quantum steering transfer within linear networks.

**1. Introduction**

Quantum steering [1–4], a typical nonlocal correlation, is a crucial quantum resource in quantum information science [5]. Unlike other correlations such as quantum entanglement [6–9] and Bell nonlocality [10], it is intrinsic asymmetry [11–14], which leads to the birth of one-way steering [15, 16] and two-way steering. Due to this asymmetry, quantum steering has been widely investigated in semi-device-independent entanglement detection [17], one-sided device-independent quantum key distribution [18–20], randomness certification [21, 22], one-sided randomness generation [23], channel discrimination [24, 25], semi-device-independent and device-independent quantification of measurement incompatibility [26, 27], secret sharing [28–30], and secure quantum teleportation [31–33]. To characterize quantum steering, various steering criteria have been proposed, including linear steering inequalities [34–40], entropic uncertainty relations [41–43], correlation matrices [44, 45], steerable weight [46, 47], steering radius [48–50], critical radius [51, 52] and steering robustness [25]. Among these, the critical radius is an unconditionally sufficient and necessary steering criterion for two-party quantum states. This is due to the fact that critical radius provides a more stringent boundary between steering and unsteering, that is, critical radius can be used to detect all one-way and two-way steerable states from two-party states.

In addition, quantum steering, as well as quantum entanglement and Bell nonlocality, unveils rich structures in multipartite configurations, particularly within the context of quantum networks [53]. Specifically, the generation of quantum entanglement in initial networks is limited in range, which means that entangled states are established along the edges between adjacent nodes. This situation can be significantly improved via entanglement swapping operations, such as quantum repeaters [54], Bell state measurements [55–57], positive-operator-valued measurements (POVM) [58, 59], and quantum

channels [60, 61], on intermediate nodes [56]. Bej *et al* [58] investigated the generation of quantum correlations of the pair (1,4), encompassing quantum entanglement, three-measurement steering, and Bell nonlocality. This was achieved through the implementation of a POVM on the pair (2,3), whose process was starting from two independent Bell pairs (1,2) and (3,4). Similarly, Qi *et al* [59] conducted analogous research within a chain-type quantum network. Their results indicate that quantum correlations can be effectively controlled by manipulating the parameters of the POVM. In addition, the concept of network quantum steering based on network local hidden state models [62] has been proposed in a linear network consisting of trusted end points, intermediate untrusted parties, and fixed measurements on untrusted parties. This network is capable of remotely transmitting quantum entanglement and steering. However, achieving one-way or two-way steering between two remote qubits, along with the perfect transfer of steerability, remains a significant challenge within quantum networks, due to the limitations posed by currently existing sufficient and unnecessary steering criteria.

Motivated by this, we propose a linear quantum network involving adjustable projection measurements on intermediate parties, which is used to achieving steerability between two endpoints. Here, we use the sufficient and necessary steering criterion i.e. critical radius [51], to quantify the steerability. In our setup, forward steering, that is, the steerability of the first entangled source can be perfectly transferred to the steerability from the first qubit to the last one in a linear quantum network, which is independent of the number of the intermediate parties and the measurements. But for the backward steering, that is, the steerability from the last qubit to the first one in the network, its pattern versus measurement parameters displays a four-leaf clovers with abundant symmetries, which can be tuned by the parameters  $\{\beta_j\}_{j=2}^N$  of the input state. With increasing the measurements, we find that the translation symmetry is broken and tunable quantum steering, i.e. one-way or two-way steering, can be realized by adjusting the measurement parameters  $\{\theta_j\}_{j=1}^{N-1}$  close to or far away from the optimal points  $\{\theta_j^{\text{opt}}\}_{j=1}^{N-1}$ . By taking further into account the measurement error, we show that the network with multiple measurements tolerates small errors for non-vanishing backward steering. This indicates that tunable steerability can be engineered by controlling measurement errors. Our study provides a potential path to achieve tunable quantum steering and manipulate its direction in linear networks.

## 2. Model and critical radius

A quantum network, as shown in figure 1, comprises entangled sources of  $N$  pairs. Initially, we prepare the input state of the quantum network into a product state of all individual entangled sources, i.e.

$\rho_{\text{in}} = \otimes_{j=1}^N \rho_{A_j B_j}$ . Then, we perform a sequence of joint measurements on all intermediate qubits. By tracing out all the intermediate qubits, the output state of the quantum network can be written as

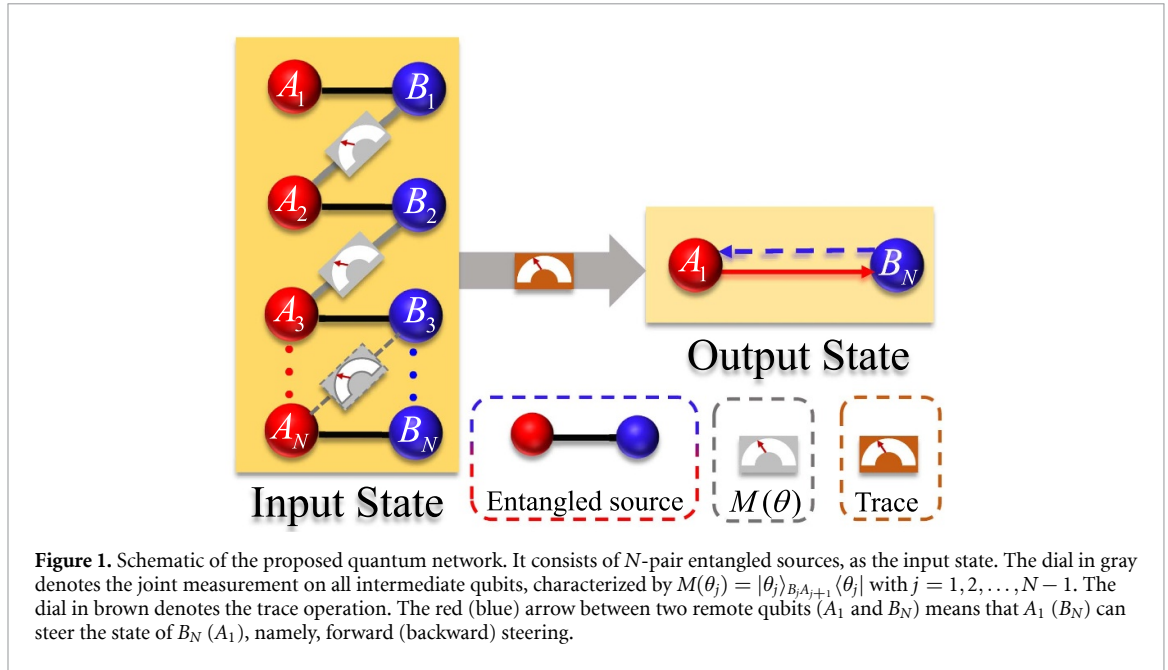
$$\rho_{\text{out}} = \frac{1}{P} \text{Tr}_{B_1 \dots B_{N-1} A_2 \dots A_N} \left[ \rho_{\text{in}} \otimes_{j=1}^{N-1} M(\theta_j) \right], \quad (1)$$

where  $P = \text{Tr}[\rho_{\text{in}} \otimes_{j=1}^{N-1} M(\theta_j)]$  is the normalized factor and  $M(\theta_j) = |\theta_j\rangle_{B_j A_{j+1}} \langle \theta_j|$  is  $j$ th joint measurement operator. The state  $|\theta_j\rangle_{B_j A_{j+1}} = \cos \theta_j |00\rangle_{B_j A_{j+1}} + \sin \theta_j |11\rangle_{B_j A_{j+1}}$ , with  $\theta_j \neq k\pi/2$  ( $k = 0, 1, 2, \dots$ ), is actually a Bell-like state. But when we set  $\theta_j = (2k+1)\pi/4$ ,  $|\theta_j\rangle_{B_j A_{j+1}}$  becomes the Bell state, and the corresponding joint measurement  $M(\theta_j)$  reduces to the Bell state measurement.

Since our goal is to realize a one-way or two-way steering between two remote qubits ( $A_1$  and  $B_N$ ) in the proposed network, a critical radius [51] is introduced to quantify it. Specifically, for an arbitrary two-qubit state  $\rho_{XY}$ , the critical radius describing the steering from  $X$  to  $Y$  is defined as

$$R_{X \rightarrow Y} = \max_{\mu} \left\{ \min_O \frac{\int_{\eta \in \mathcal{B}_Y} d\mu(\eta) |\text{Tr}(O\eta)|}{\sqrt{2} \|\text{Tr}_Y[\bar{\rho}_{XY}(I \otimes O)]\|} \right\}, \quad (2)$$

where  $O = \frac{1}{2}(o_0 I + \vec{o} \cdot \vec{\sigma})$ , with  $\vec{\sigma} = (\sigma_x, \sigma_y, \sigma_z)$ , is a single-qubit observable,  $\mu$  is a distribution over states  $\eta = \frac{1}{2}(I + \vec{v} \cdot \vec{\sigma})$  in the Bloch ball  $\mathcal{B}_Y$ , and  $\bar{\rho}_{XY} = \rho_{XY} - \frac{1}{2} \otimes \rho_Y$ . Equation (2) indicates that the state  $\rho_{XY}$  is steerable from  $X$  to  $Y$  only when  $R_{X \rightarrow Y} < 1$ . To further establish the region of the critical radius, we take a generalized Bell diagonal state, i.e.  $\rho_{\text{bds}} = \frac{1}{4}(I \otimes I + t_x \sigma_x \otimes \sigma_x + t_y \sigma_y \otimes \sigma_y + t_z \sigma_z \otimes \sigma_z)$ , as an example, but



without loss of generality to calculate it. By choosing the optimal observable and distribution,

$$R_{X \rightarrow Y}(\rho_{\text{bds}}) = \frac{2\pi |t_x t_y t_z|}{\int \left( t_x^{-2} n_x^2 + t_y^{-2} n_y^2 + t_z^{-2} n_z^2 \right)^{-2} dS} \quad (3)$$

is obtained, where  $n_x = \sin \alpha \cos \varphi$ ,  $n_y = \sin \alpha \sin \varphi$ ,  $n_z = \cos \alpha$ , and  $dS = \sin \alpha d\alpha d\varphi$ . Equation (3) directly gives  $R_{X \rightarrow Y} = 1/2$  for the Bell state ( $t_x = -t_y = t_z = 1$ ) and  $R_{X \rightarrow Y} \rightarrow \infty$  for the maximally mixed state ( $t_x = t_y = t_z = 0$ ), corresponding to the lower and upper limits of the critical radius. Therefore, the critical radius  $R_{X \rightarrow Y}$  is limited to the region of  $[1/2, \infty)$ . This steerable zone can be in the region of  $[0, 1]$  by redefining the critical radius,

$$\mathcal{R}_{X \rightarrow Y} = \max \{0, R_{X \rightarrow Y}^{-1} - 1\}, \quad (4)$$

which indicates that the state  $\rho_{XY}$  from  $X$  to  $Y$  is steerable when  $\mathcal{R}_{X \rightarrow Y} > 0$ , or equivalently  $R_{X \rightarrow Y} < 1$ .

### 3. Tunable steerability in quantum network

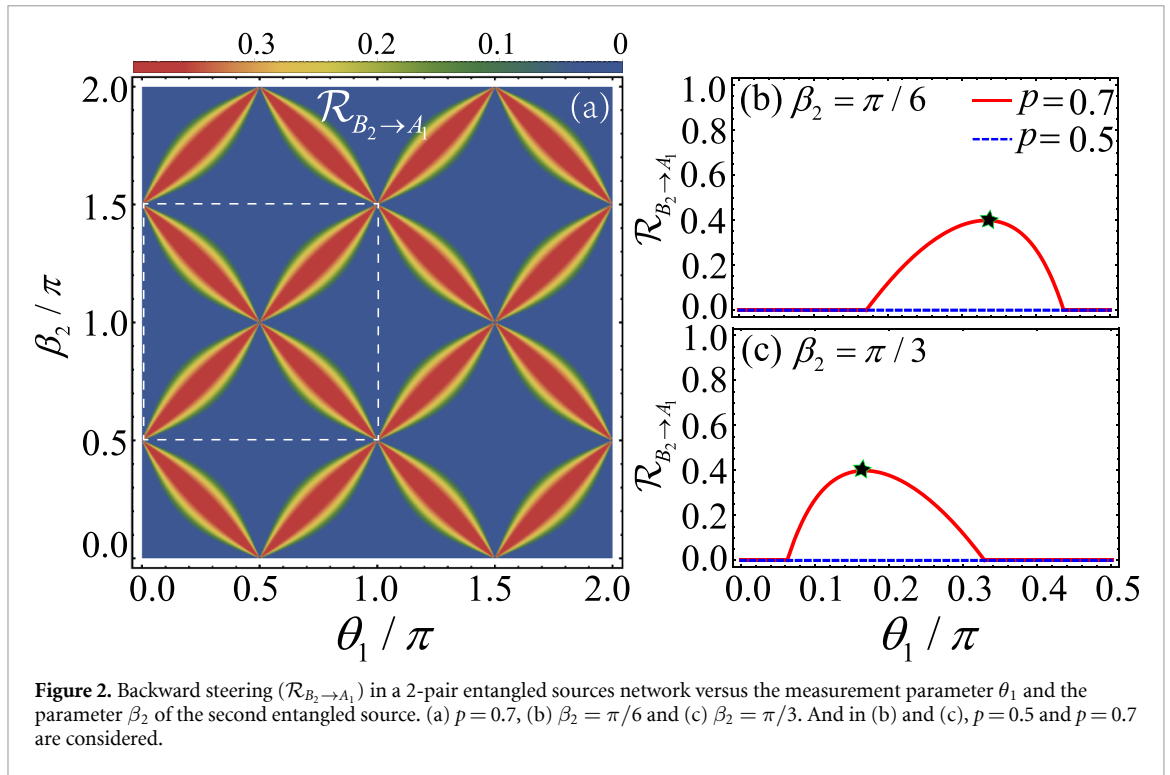
Next, we assume that parties  $A_1$  and  $B_1$  share an entangled Werner state ( $p > 1/3$ )

$$\rho_{A_1 B_1} = p |\text{Bell}\rangle_{A_1 B_1} \langle \text{Bell}| + (1-p) \frac{I_{A_1}}{2} \otimes \frac{I_{B_1}}{2}, \quad (5)$$

and other parties  $A_j$  and  $B_j$  are in an entangled pure state

$$\rho_{A_j B_j} = |\beta_j\rangle_{A_j B_j} \langle \beta_j| \quad \text{with } j = 2, 3, \dots, N, \quad (6)$$

where  $|\beta_j\rangle_{A_j B_j} = \cos \beta_j |00\rangle_{A_j B_j} + \sin \beta_j |11\rangle_{A_j B_j}$  and  $|\text{Bell}\rangle_{A_1 B_1} = |\pi/4\rangle_{A_1 B_1}$ . From equation (3), one can see that the critical radii of the state  $\rho_{A_1 B_1}$  from  $A_1 \rightarrow B_1$  and  $B_1 \rightarrow A_1$  are equal, that is,  $R_{A_1 \rightarrow B_1} = R_{B_1 \rightarrow A_1} = (2p)^{-1}$ . As a result, the state  $\rho_{A_1 B_1}$  is two-way (no-way) steerable for  $p > 1/2$  ( $p \leq 1/2$ ). The term ‘no-way steerable’ here refers to the quantum state being unsteerable in both directions. But for an entangled pure state  $\rho_{A_j B_j}$  given by equation (6), it is obviously two-way steerable [37, 51]. This indicates that there is no steering between remote parties  $A_1$  and  $B_N$  without additional operations. In other words, a set of joint measurements is required to establish the steerability between these two parities. Taking advantage of the critical radius, we demonstrate that the steering direction between two remote parties ( $A_1$  and  $B_N$ ) can be changed by adjusting the measurement parameters  $\{\theta_j\}_{j=1}^{N-1}$ . For further clarity, we include a detailed investigation of the following examples.



### 3.1. Two entangled sources

We first show how to realize one-way and two-way steering between two parties ( $A_1$  and  $B_2$ ) in the simplest network, consisting of two entangled sources, i.e.  $N = 2$ . In this case, only one joint measurement  $M(\theta_1)$  is imposed. For a given input state (see equations (5) and (6)), the output state is (see details in appendix A)

$$\rho_{A_1 B_2}^{\text{out}} = p \psi_{A_1 B_2} + (1-p) \frac{I_{A_1}}{2} \otimes \psi_{B_2}, \quad (7)$$

where  $\psi_{A_1 B_2} = |g_2\rangle_{A_1 B_2} \langle g_2|$  is an entangled pure state, and  $\psi_{B_2} = \text{Tr}_{A_1}(\psi_{A_1 B_2})$  is the reduced density matrix. In the above expressions,  $|g_2\rangle_{A_1 B_2} = \cos g_2 |00\rangle_{A_1 B_2} + \sin g_2 |11\rangle_{A_1 B_2}$ , with the  $g$ -function

$$g_2 = \frac{1}{2} \arccos \left( 1 - \frac{2}{1 + \cot^2 \beta_2 \cot^2 \theta_1} \right). \quad (8)$$

For the output state  $\rho_{A_1 B_2}^{\text{out}}$ , its critical radius from  $A_1$  to  $B_2$  is  $R_{A_1 \rightarrow B_2} = (2p)^{-1}$  (see details in appendix B), which is the same as the critical radius of the input state  $\rho_{A_1 B_1}$  from  $A_1$  to  $B_1$ . This means that the steerability of the state  $\rho_{A_1 B_1}$  from  $A_1$  to  $B_1$  can be perfectly transferred to the steerability of the state  $\rho_{A_1 B_2}^{\text{out}}$  from  $A_1$  to  $B_2$ . For the critical radius  $R_{B_2 \rightarrow A_1}$  of the state  $\rho_{A_1 B_2}^{\text{out}}$ , it can not be given analytically. Fortunately, it can be numerically investigated with equation (2) (see details in appendix B). To show the numerical result, we plot the redefining critical radius  $\mathcal{R}_{B_2 \rightarrow A_1}$  as functions of parameters  $\theta_1$  and  $\beta_2$  in figure 2(a) with  $p = 0.7$ . Intuitively, the pattern resembles *four-leaf clovers* having central-, axial-, rotational and translation-symmetry (see the dashed box), which can be attributed to the periodic nature of the cotangent function in equation (8). The leaf denotes the steerability from  $B_2$  to  $A_1$  of the output state, and the non-leaf part denotes no steerability from  $B_2$  to  $A_1$ . Obviously, an optimal steering exists (see the pattern in red) and we can tune parameters  $\theta_1$  and  $\beta_2$  to achieve it. For clarity, we further plot  $\mathcal{R}_{B_2 \rightarrow A_1}$  versus the parameter  $\theta_1 \in (0, \pi/2)$  with fixed  $\beta_2 = \pi/6$  and  $\pi/3$  in figures 2(b) and (c), respectively. The unsteerable input state  $\rho_{A_1 B_1}$  with  $p = 1/2$  (see discussions after equation (6)) leads to the output state  $\rho_{A_1 B_2}^{\text{out}}$  unsteerable (no-way steering), as demonstrated by the blue curves. When we take  $p > 1/2$  such as  $p = 0.7$ , the input state  $\rho_{A_1 B_1}$  becomes steerable, giving rise to one-way or two-way steering for the output state  $\rho_{A_1 B_2}^{\text{out}}$  (see the red curves). This suggests that both one-way and two-way steering can be obtained by tuning the measurement parameter  $\theta_1$  for a definite steerable input state  $\rho_{A_1 B_1}$ . Moreover, we find that the optimal steerability of the output state  $\rho_{A_1 B_2}^{\text{out}}$  can be achieved under an optimal measurement  $M(\theta_1^{\text{opt}})$  (see green stars in figures 2(b) and (c)), where

$$\theta_1^{\text{opt}} = \frac{\pi}{2} - \beta_2. \quad (9)$$

The optimal measurement yields the same output state as the input state  $\rho_{A_1B_1}$ . This implies that the steerable input state can be perfectly transferred to the output state with the optimal measurement. From figure 2(a), one can see that one-way and two-way steering for the output state can also be attained by tuning the parameter  $\beta_2$  with the fixed  $\theta_1$ , which is consistent with  $g_2$  given by equation (8).

### 3.2. Three entangled sources

In the following, we expand the network to the case of  $N = 3$ . In this scenario, the input state can be considered not only as the product of three individual entangled sources but also as the product state of the third entangled source and the output state of the first two entangled sources. Clearly, these two perspectives are equivalent. However, from the latter perspective, the scenario for  $N = 3$  can be directly reduced to that of  $N = 2$ , except for the inclusion of an additional measurement  $M(\theta_2)$  on parties  $B_2$  and  $A_3$  and the introduction of a variable parameter  $\beta_3$ . This results in a network comprising three entangled sources that are more adjustable. Following the procedure in appendix A, the output state of the network can be expressed as

$$\rho_{A_1B_3}^{\text{out}} = p\psi_{A_1B_3} + (1-p)\frac{I_{A_1}}{2} \otimes \psi_{B_3}, \quad (10)$$

where  $\psi_{A_1B_3} = |g_3\rangle_{A_1B_3}\langle g_3|$  and  $\psi_{B_3} = \text{Tr}_{A_1}(\psi_{A_1B_3})$ . The  $g$ -function is

$$g_3 = \frac{1}{2} \arccos \left( 1 - \frac{2}{1 + \prod_{j=1}^2 \cot^2 \theta_j \cot^2 \beta_{j+1}} \right). \quad (11)$$

Apparently, the steerability of the output state  $\rho_{A_1B_3}^{\text{out}}$  from  $A_1$  to  $B_3$  is  $R_{A_1 \rightarrow B_3} = (2p)^{-1}$ , which is the same as  $R_{A_1 \rightarrow B_2}$  because of their similar forms. This indicates that the steerability from  $A_1$  to  $B_1$  of the input state  $\rho_{A_1B_1}$  can be perfectly transferred to the steerability from  $A_1$  to  $B_3$  of the output state  $\rho_{A_1B_3}^{\text{out}}$ . For the backward steering from  $B_3$  to  $A_1$ , we find that its pattern, as functions of  $\theta_1$  and  $\theta_2$  in figure 3, displays four-leaf clovers with *adjustable* symmetry (see the dashed box) by tuning the parameter  $\beta$  ( $\beta_2 = \beta_3 = \beta$  are assumed) for fixed  $p$ , which is different from the case of  $N = 2$ . Specifically, when  $\beta = \pi/4$ , the second and third entangled sources are in an symmetric state, i.e. Bell state, giving rise to symmetric pattern similar to the case of  $N = 2$  (see figures 3(b) and (e)). But when  $\beta = \pi/6$  or  $\pi/3$ , the steerability of the output state from  $B_3$  to  $A_1$  only keeps axial-, rotational-, and central-symmetry, while the translation-symmetry is broken (see figures 3(a)–(f)). This is because that the second and third entangled sources are in the unsymmetric Bell-like state in the cases of  $\beta \neq (2k+1)\pi/4$  ( $k = 0, 1, 2, \dots$ ). In addition, we find that neighboring leaves for a four-leaf clover along  $\theta_2$ -( $\theta_1$ -) direction exhibit repulsion (attraction) from each other for  $\beta = \pi/6$  (see figures 3(a) and (d)). But when  $\beta = \pi/3$ , the situation is fully reversed (see figures 3(c) and (f)). It is evident that a larger value of  $p$  results in both a larger steering zone and a larger optimal value by comparing the first and second panels. This is because the input state described by equation (5) approaches the Bell state more closely as  $p$  increases. From figure 3, we further confirm that optimal backward steering can be periodically predicted at

$$\theta_1^{\text{opt}} = \pi/2 - \beta_2 \quad \text{and} \quad \theta_2^{\text{opt}} = \pi/2 - \beta_3. \quad (12)$$

The periodicity can also be roughly predicted from  $g$ -function given by equation (11). As the backward steering can be tuned from zero to its optimal value, so one-way and two-way steering of the output state can be achieved in a controlled manner.

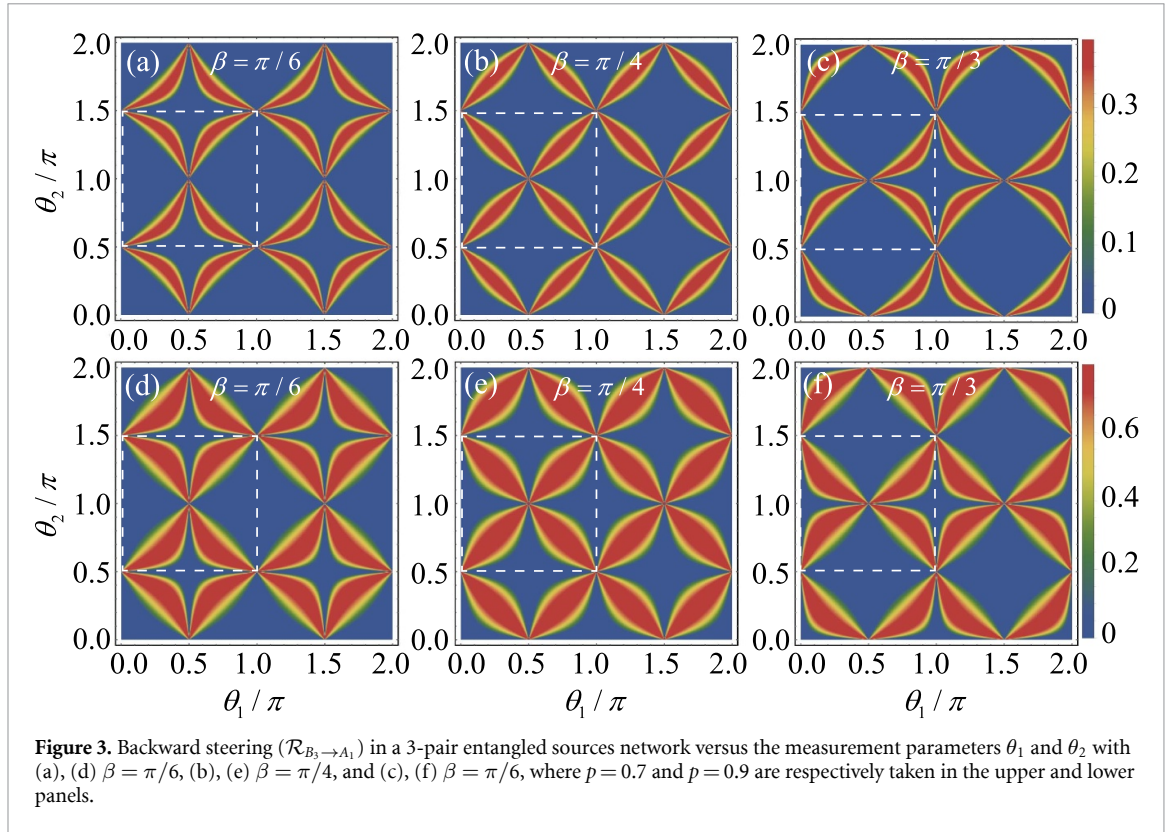
### 3.3. Multiple entangled sources

In this part, we further consider that the network is extended to the case of  $N$ -pair entangled sources, where the first source is in a Werner state and each of the rest is in a Bell-like state. By utilizing the inductive method based on the cases of  $N = 2$  and 3, the output state can be written as

$$\rho_{A_1B_N}^{\text{out}} = p\psi_{A_1B_N} + (1-p)\frac{I_{A_1}}{2} \otimes \psi_{B_N}, \quad (13)$$

where  $\psi_{A_1B_N} = |g_N\rangle_{A_1B_N}\langle g_N|$  with  $|g_N\rangle_{A_1B_N} = \cos g_N |00\rangle_{A_1B_N} + \sin g_N |11\rangle_{A_1B_N}$ , and  $\psi_{B_N} = \text{Tr}_{A_1}(\psi_{A_1B_N})$ . The  $g$ -function here is given by

$$g_N = \frac{1}{2} \arccos \left( 1 - \frac{2}{1 + \prod_{j=1}^{N-1} \cot^2 \theta_j \cot^2 \beta_{j+1}} \right). \quad (14)$$



**Figure 3.** Backward steering ( $\mathcal{R}_{B_N \rightarrow A_1}$ ) in a 3-pair entangled sources network versus the measurement parameters  $\theta_1$  and  $\theta_2$  with (a), (d)  $\beta = \pi/6$ , (b), (e)  $\beta = \pi/4$ , and (c), (f)  $\beta = \pi/3$ , where  $p = 0.7$  and  $p = 0.9$  are respectively taken in the upper and lower panels.

According to the results in the cases of  $N = 2$  and  $N = 3$ , the critical radius of the output state  $\rho_{A_1 B_N}^{\text{out}}$  from  $A_1$  to  $B_N$  is  $R_{A_1 \rightarrow B_N} = (2p)^{-1} = R_{A_1 \rightarrow B_1}$ . This indicates that the steerability from  $A_1$  to  $B_1$  can always be perfectly transferred to the steerability from  $A_1$  to  $B_N$ , regardless of the number of intermediate parties and the measurement. However, for the backward steering from  $B_N$  to  $A_1$ , its critical radius  $R_{B_N \rightarrow A_1}$  is severely affected by the unoptimal measurement number. These two situations are numerically shown in figure 4(a), respectively, denoted by red circles and squares. The corresponding parameters are  $p = 0.9$ ,  $\beta = \beta_2 = \dots = \beta_N = \pi/6$ , and  $\theta = \theta_1 = \theta_2 = \dots = \theta_{N-1}$ . Apparently, the backward steering decreases with increasing measurement number. With the parameter  $\theta = \pi/6$  adopted in figure 4(a), one can see that  $\mathcal{R}_{B_N \rightarrow A_1} = 0$  when  $N = 3$ . This means that the output state  $\rho_{A_1 B_N}^{\text{out}}$  is two-way (one-way) steering when  $N < 3$  ( $N \geq 3$ ). For a more complicated network, more measurements ( $N \geq 4$ ) are required for achieving one (two)-way steering between two remote parties ( $A_1$  and  $B_N$ ). This can be realized by tuning measurement parameters in proximity to the optimal value, i.e.

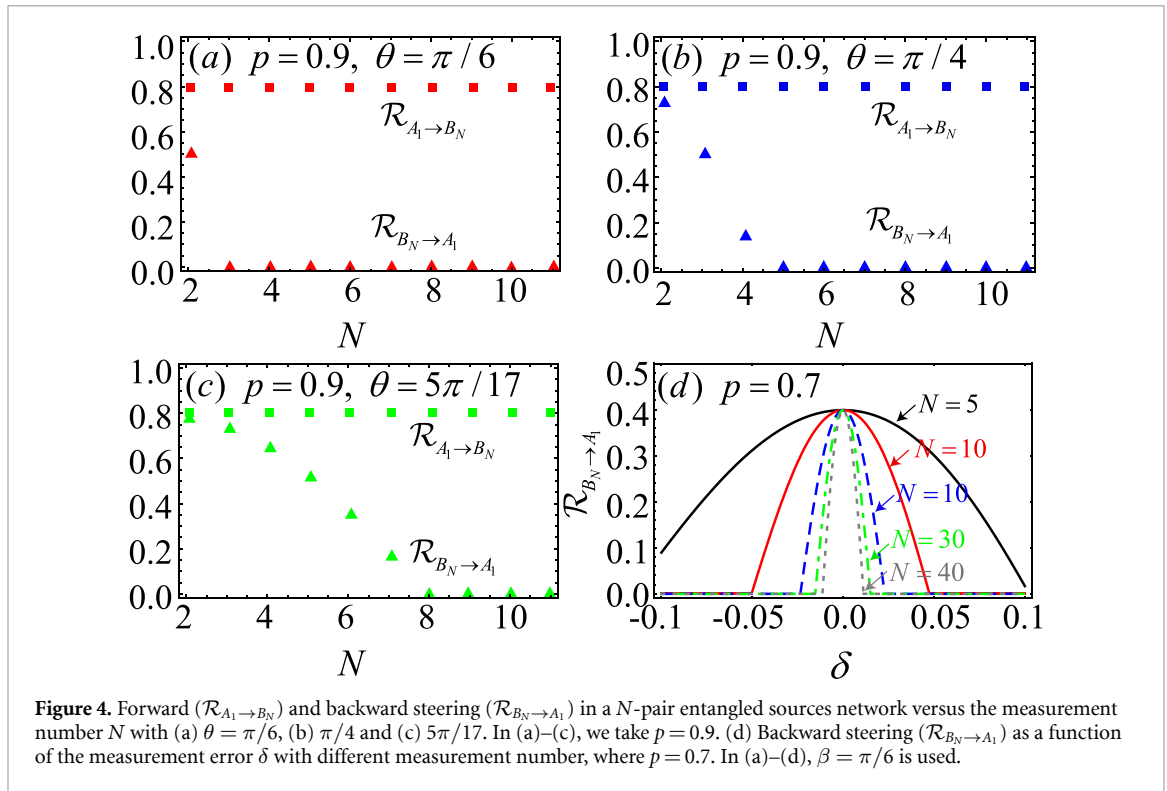
$$\theta_j^{\text{opt}} = \frac{\pi}{2} - \beta_{j+1} \quad \text{with } j = 1, 2, \dots, N-1, \quad (15)$$

as demonstrated by blue ( $\theta = \pi/4$ ) and green ( $\theta = 5\pi/17$ ) markers in figures 4(b) and (c), where the optimal value  $\theta^{\text{opt}} = \pi/3$  because of  $\beta = \pi/6$ .

In practice, optimal measurements cannot be made accurately. Therefore, the error ( $\delta$ ) between actual measurements ( $\theta^{\text{act}}$ ) and the optimal measurements ( $\theta^{\text{opt}}$ ) must be taken into account, which can be defined as

$$\delta = \theta^{\text{act}} / \theta^{\text{opt}} - 1. \quad (16)$$

In figure 4(d), we plot the backward steering ( $\mathcal{R}_{B_N \rightarrow A_1}$ ) versus the measurement error with different measurement number  $N$ , where  $p = 0.7$  and  $\beta = \pi/6$ . Clearly,  $\mathcal{R}_{B_N \rightarrow A_1}$  can present with a larger error when the measurements are fewer, such as  $N = 5$  (see the black curve). By gradually adding the number of measurements, for example, from  $N = 10$  to  $N = 40$ , the smaller and smaller error is allowed for non-vanishing backward steering. These indicate that as the number of measurements increases, the critical measurement error corresponding to the disappearance of the backward steering becomes smaller. In other words, the realization of two-way (one-way) steering in a many-body network requires measurements close to (away from) the optimal points when other parameters are fixed.



#### 4. Conclusion

In summary, we propose a promising way to realize one-way and two-way steering between two remote parties ( $A_1$  and  $B_N$ ) in a linear quantum network by performing the joint measurements  $\{M(\theta_j)\}_{j=1}^{N-1}$  on all intermediate parties. In our scheme, the reason for choosing the Werner state as the first entangled source is that: (1) the forward steering is the same as the backward steering; (2) after performing the joint measurements, the output state of the quantum network has a certain regularity, which can be obtained for the case of  $N \geq 4$  through mathematical induction. By using the necessary and sufficient criterion (i.e. the critical radius), we find that the forward steering can always be perfectly transferred from the first entangled source to two endpoints, regardless of the number of the intermediate parties and the measurements. For the backward steering, its pattern behaves like a four-leaf clovers with rich symmetries, which is dependence of the input state of the network. With increasing the number of measurements, this means that the quantum network is formed by  $N$  ( $N \geq 4$ ) entangled sources and  $N - 1$  joint measurements. We can show that not only the translation-symmetry of the pattern is broken, but also one-way and two-way steering can be obtained by tuning measurement parameters. We also consider the impact of the measurement error on the backward steering. Our work paves the way for a potential way to build the one-way and two-way steering with multiple measurements within the directional network.

#### Data availability statement

All data that support the findings of this study are included within the article (and any supplementary files).

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## Appendix A. The derivation of the output state in equation (7)

For the case of  $N = 2$ , we take the product of an entangled Werner state  $\rho_{A_1B_1}$  and an entangled pure state  $\rho_{A_2B_2}$  as the input state. By performing the measurement  $M(\theta_1)$  and tracing out the untrusted parties  $B_1$  and  $A_2$ , the unnormalized output state can be expressed as

$$\begin{aligned}\sigma_{A_1B_2}^{\text{out}} &= \text{Tr}_{B_1A_2} [\rho_{A_1B_1} \otimes \rho_{A_2B_2} M(\theta_1)] \\ &= p\phi_{A_1B_2} + (1-p)\frac{I_{A_1}}{2} \otimes \sigma_{B_2},\end{aligned}\quad (\text{A.1})$$

where

$$\begin{aligned}\phi_{A_1B_2} &= \text{Tr}_{B_1A_2} [|\text{Bell}\rangle_{A_1B_1} \langle \text{Bell}| \otimes \rho_{A_2B_2} M(\theta_1)], \\ \sigma_{B_2} &= \text{Tr}_{B_1A_2} \left[ \frac{I_{B_1}}{2} \otimes \rho_{A_2B_2} M(\theta_1) \right].\end{aligned}\quad (\text{A.2})$$

As the measurement  $M(\theta_1)$  is performed on the untrusted parties  $B_1$  and  $A_2$ , so  $\sigma_{B_2} = \text{Tr}_{A_1} [\phi_{A_1B_2}] \equiv \phi_{B_2}$ . Thus,  $\sigma_{A_1B_2}^{\text{out}}$  in equation (A.1) reduces to

$$\sigma_{A_1B_2}^{\text{out}} = p\phi_{A_1B_2} + (1-p)\frac{I_{A_1}}{2} \otimes \phi_{B_2}.\quad (\text{A.3})$$

We then go to establish the specific form of the state  $\phi_{A_1B_2}$  in equation (A.3). For this, the following four measurement basis for parties  $B_1$  and  $A_2$  are employed,

$$\begin{aligned}|\psi_1\rangle_{B_1A_2} &= \cos\theta_1|00\rangle_{B_1A_2} + \sin\theta_1|11\rangle_{B_1A_2}, \\ |\psi_2\rangle_{B_1A_2} &= \sin\theta_1|00\rangle_{B_1A_2} - \cos\theta_1|11\rangle_{B_1A_2}, \\ |\psi_3\rangle_{B_1A_2} &= \cos\theta_1|01\rangle_{B_1A_2} + \sin\theta_1|10\rangle_{B_1A_2}, \\ |\psi_4\rangle_{B_1A_2} &= \sin\theta_1|01\rangle_{B_1A_2} - \cos\theta_1|10\rangle_{B_1A_2},\end{aligned}\quad (\text{A.4})$$

or equivalently,

$$\begin{aligned}|00\rangle_{B_1A_2} &= \cos\theta_1|\psi_1\rangle_{B_1A_2} + \sin\theta_1|\psi_2\rangle_{B_1A_2}, \\ |11\rangle_{B_1A_2} &= \sin\theta_1|\psi_1\rangle_{B_1A_2} - \cos\theta_1|\psi_2\rangle_{B_1A_2}, \\ |01\rangle_{B_1A_2} &= \cos\theta_1|\psi_3\rangle_{B_1A_2} + \sin\theta_1|\psi_4\rangle_{B_1A_2}, \\ |10\rangle_{B_1A_2} &= \sin\theta_1|\psi_3\rangle_{B_1A_2} - \cos\theta_1|\psi_4\rangle_{B_1A_2}.\end{aligned}\quad (\text{A.5})$$

With these basis, we have

$$\begin{aligned}|\text{Bell}\rangle_{A_1B_1} \otimes |\beta_2\rangle_{A_2B_2} &= |\phi_1\rangle_{A_1B_2} \otimes |\psi_1\rangle_{B_1A_2} + |\phi_2\rangle_{A_1B_2} \otimes |\psi_2\rangle_{B_1A_2} \\ &\quad + |\phi_3\rangle_{A_1B_2} \otimes |\psi_3\rangle_{B_1A_2} + |\phi_4\rangle_{A_1B_2} \otimes |\psi_4\rangle_{B_1A_2},\end{aligned}\quad (\text{A.6})$$

where

$$\begin{aligned}|\phi_1\rangle_{A_1B_2} &= \frac{1}{\sqrt{2}} (\cos\beta_2 \cos\theta_1 |00\rangle + \sin\beta_2 \sin\theta_1 |11\rangle)_{A_1B_2}, \\ |\phi_2\rangle_{A_1B_2} &= \frac{1}{\sqrt{2}} (\cos\beta_2 \sin\theta_1 |00\rangle - \sin\beta_2 \cos\theta_1 |11\rangle)_{A_1B_2}, \\ |\phi_3\rangle_{A_1B_2} &= \frac{1}{\sqrt{2}} (\sin\beta_2 \cos\theta_1 |01\rangle + \cos\beta_2 \sin\theta_1 |10\rangle)_{A_1B_2}, \\ |\phi_4\rangle_{A_1B_2} &= \frac{1}{\sqrt{2}} (\sin\beta_2 \sin\theta_1 |01\rangle - \cos\beta_2 \cos\theta_1 |10\rangle)_{A_1B_2}.\end{aligned}$$

When  $M(\theta_1) = |\theta\rangle_{B_1A_2} \langle \theta| = |\psi_1\rangle_{B_1A_2} \langle \psi_1|$  is applied to parties  $B_1$  and  $A_2$ , the state in equation (A.6) collapses to  $|\phi_1\rangle_{A_1B_2} \otimes |\psi_1\rangle_{B_1A_2}$ . By tracing out  $B_1$  and  $A_2$ , we have

$$\phi_{A_1B_2} = |\phi_1\rangle_{A_1B_2} \langle \phi_1|. \quad (\text{A.7})$$

Once equation (A.7) is obtained, the output state  $\rho_{A_1 B_2}^{\text{out}}$  can be calculated following the normalization procedure, i.e.

$$\rho_{A_1 B_2}^{\text{out}} = \frac{\sigma_{A_1 B_2}^{\text{out}}}{\text{Tr}(\sigma_{A_1 B_2}^{\text{out}})} = p\psi_{A_1 B_2} + (1-p)\frac{I_{A_1}}{2} \otimes \psi_{B_2}, \quad (\text{A.8})$$

with

$$\begin{aligned} \psi_{A_1 B_2} &= \frac{\phi_{A_1 B_2}}{\text{Tr}(\phi_{A_1 B_2})} = |g_2\rangle_{A_1 B_2} \langle g_2|, \\ \psi_{B_2} &= \frac{\phi_{B_2}}{\text{Tr}(\phi_{B_2})} = \text{Tr}_{A_1}(\psi_{A_1 B_2}), \\ |g_2\rangle_{A_1 B_2} &= \cos g_2 |00\rangle_{A_1 B_2} + \sin g_2 |11\rangle_{A_1 B_2}, \end{aligned} \quad (\text{A.9})$$

where  $g_2 = \frac{1}{2} \arccos\left(1 - \frac{2}{1 + \cot^2 \beta_2 \cot^2 \theta_1}\right)$  is the  $g$ -function.

## Appendix B. The calculation of the critical radii for the output state in equation (13)

For the critical radius  $R_{A_1 \rightarrow B_N}$  of the state  $\rho_{A_1 B_N}^{\text{out}}$ , it has the analytical solution. In order to obtain of the analytical solution, we first introduce one property of the critical radius [51].

Property—For an arbitrary two-qubit state  $\rho$ , consider a local reversible operation  $V_B$ , and apply this operation  $V_B$  to the original state to obtain a new state

$$\rho' = \frac{(I_A \otimes V_B) \rho (I_A \otimes V_B)^\dagger}{\text{Tr}[(I_A \otimes V_B) \rho (I_A \otimes V_B)^\dagger]}. \quad (\text{B.1})$$

For these two states, their critical radii satisfy the relation  $R_{A \rightarrow B}(\rho') = R_{A \rightarrow B}(\rho)$ .

By using the property, we consider a local reversible operation  $V_{B_N} = [\text{Tr}_{A_1}(\rho_{A_1 B_N}^{\text{out}})]^{-\frac{1}{2}}$ , apply this operation to the output state  $\rho_{A_1 B_N}^{\text{out}}$  to obtain a new state

$$\rho'_{A_1 B_N} = \frac{(I_{A_1} \otimes V_{B_N}) \rho_{A_1 B_N}^{\text{out}} (I_{A_1} \otimes V_{B_N})^\dagger}{\text{Tr}[(I_{A_1} \otimes V_{B_N}) \rho_{A_1 B_N}^{\text{out}} (I_{A_1} \otimes V_{B_N})^\dagger]}. \quad (\text{B.2})$$

Through rigorous mathematical calculations, we find that this new state  $\rho'_{A_1 B_N}$  is a Werner state, and the same as for the first entangled source, which shows that the critical radius of the output state can be given by  $R_{A_1 \rightarrow B_N}(\rho_{A_1 B_N}^{\text{out}}) = (2p)^{-1}$ . Thus, the forward steering  $\mathcal{R}_{A_1 \rightarrow B_N} = \max\{0, R_{A_1 \rightarrow B_N}^{-1} - 1\} = \max\{0, 2p - 1\}$  is not affected by the performed joint-measurements  $M(\theta_j) = |\theta_j\rangle_{B_j A_{j+1}} \langle \theta_j|$  with  $j = 1, 2, \dots, N-1$ .

For the critical radius  $R_{B_N \rightarrow A_1}$  of the state  $\rho_{A_1 B_N}^{\text{out}}$ , it has no analytical solution and can only be calculated numerically using the definition of the critical radius in equation (2). Due to the large amount of computation, we only consider three cases  $p = 0.5$ ,  $p = 0.7$ ,  $p = 0.9$  and use the Taylor series fitting method to obtain the approximate expression of the negative power of the critical radius.

When  $p = 0.5$ , its fitting function is

$$\begin{aligned} R_{B_N \rightarrow A_1}^{-1} &= 0.000524371 + 6.93072x + 3.00345x^2 - 134.205x^3 \\ &\quad + 467.93x^4 - 800.941x^5 + 533.961x^6, \end{aligned} \quad (\text{B.3})$$

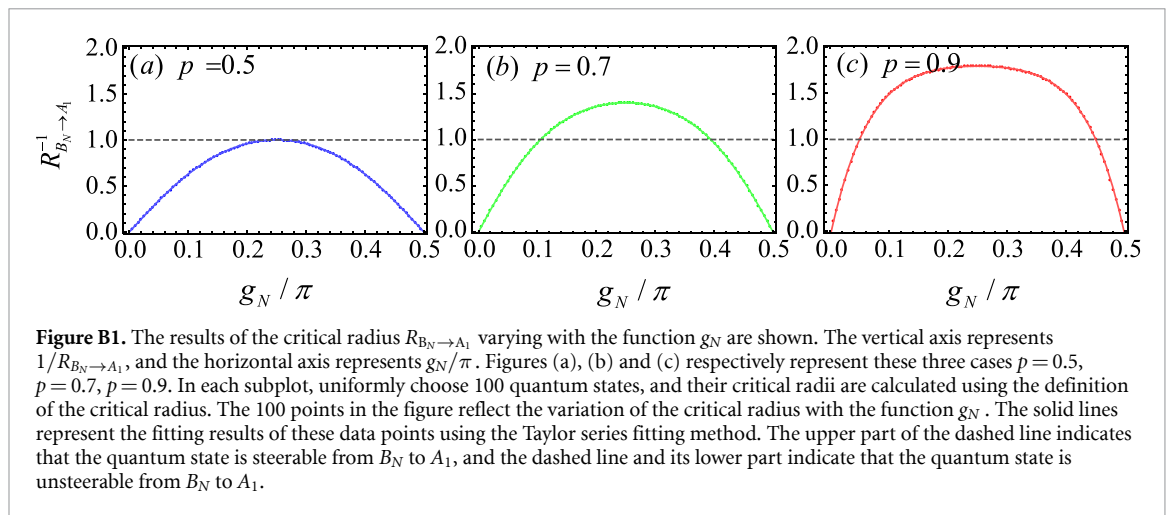
when  $p = 0.7$ , its fitting function is

$$\begin{aligned} R_{B_N \rightarrow A_1}^{-1} &= -0.00424723 + 12.0541x - 10.55x^2 - 215.743x^3 \\ &\quad + 1023.3x^4 - 1938.13x^5 + 1292.08x^6, \end{aligned} \quad (\text{B.4})$$

when  $p = 0.9$ , its fitting function is

$$\begin{aligned} R_{B_N \rightarrow A_1}^{-1} &= -0.0414525 + 29.5148x - 206.512x^2 + 821.949x^3 \\ &\quad - 1982.05x^4 + 2784.23x^5 - 1856.15x^6, \end{aligned} \quad (\text{B.5})$$

where  $x = g_N/\pi$ . The fitting results are shown in following figure B1.



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