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A fixed phase tunable directional coupler based on coupling tuning

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The field of photonic integrated circuits has witnessed significant progress in recent years, with a growing demand for devices that offer high-performance reconfigurability. Due to the inability of conventional tunable directional couplers (TDCs) to maintain a fixed phase while tuning the reflectivity, Mach-Zehnder interferometers (MZIs) are employed as the primary building blocks for reflectivity tuning in constructing large-scale circuits. However, MZIs are prone to fabrication errors due to the need for perfect balanced directional couplers to achieve 0-1 reflectivity, which hinders their scalability. In this study, we introduce a design of a TDC based on coupling constant tuning in the thin film Lithium Niobate platform and present an optimized design. Our optimized TDC design enables arbitrary reflectivity tuning while ensuring a consistent phase across a wide range of operating wavelengths. Furthermore, it exhibits fewer bending sections than MZIs and is inherently resilient to fabrication errors in waveguide geometry and coupling length compared to both MZIs and conventional TDCs. Our work contributes to developing high-performance photonic integrated circuits with implications for various fields, including optical communication systems and quantum information processing.

Photonic integrated circuits (PICs) have emerged as a promising technology for enabling complex optical functionalities with a small footprint^{1–3}. One significant advancement in PICs is the development of programmable PICs⁴, which are highly versatile devices capable of processing optical signals in a reconfigurable manner. These circuits have exhibited remarkable capabilities finding extensive applications in diverse fields, including radio-frequency signal processing⁵, machine learning^{6,7}, condensed matter physics systems simulations⁸, and quantum information processing^{9,10}. To meet the demands of more advanced applications, the integration density of PICs is increasing rapidly². The most adaptable strategies involve constructing waveguide mesh structures or multi-port universal interferometers^{11–13} based on the fundamental tunable device that realizes universal 2×2 transformation. This device is implemented by the Mach-Zehnder interferometer (MZI) with an extra phase shifter for relative phase tuning of the output states^{6,7,14–17}. Such an MZI consists of two balanced (50:50) beam splitters and a phase shifter for reflectivity tuning (Fig. 1a and d). (Reflectivity η is defined as $\eta = 1 - \kappa$, following the convention in the field of quantum optics^{18,19}, where κ represents the coupling or power transfer ratio^{20,21}.) However, employing a one-to-one component mapping approach to transferring MZIs from bulk free-space optics to PICs may not be the optimal strategy. This is because the design of MZIs is sensitive to fabrication errors and exhibits more bending losses^{22,23}. Achieving balanced directional couplers (DCs) requires perfect fabrication and is crucial for constructing MZIs to achieve 0-1 reflectivity. Additionally, each MZI has 4 bending sections (Fig. 1a), which introduces optical losses and can decrease the fidelity of larger scale circuits¹².

As an alternative to MZIs, the conventional $\Delta\beta$ -based TDC ($\Delta\beta$ -TDC) (see the illustration in Fig. 1b and an example device schematic in Fig. 2a, b), which relies on creating a difference in propagation constants between the two waveguides to tune the reflectivity, have less bending sections. However, such a device is wavelength-dependent and sensitive to fabrication error. Furthermore, both its reflectivity and phase shift are dependent on the voltage, and cannot be independently controlled^{21,24,25} (Fig. 1e). Moreover, the exact phase-voltage dependence has to be characterized after the fabrication of the device, which is experimentally challenging for high-dimensional photonic circuits, or circuits consisting of cascaded sections. In applications where phase shifts are critical (such as in quantum information processing), this will cause a degradation in the overall performance of the system.

In this paper, we propose a ΔC -based TDC (ΔC -TDC) (see the illustration in Fig. 1c and the device schematic Fig. 2c) that implements the same unitary transformation as an MZI, but possesses fewer bending sections and enhanced fabrication error tolerance, with a method to assess its performance. This addresses the scalability challenges, potentially enabling more advanced applications associated with using MZIs. Unlike conventional $\Delta\beta$ -TDCs, our ΔC -TDC design achieves tunability through coupling tuning, which maintains the relative

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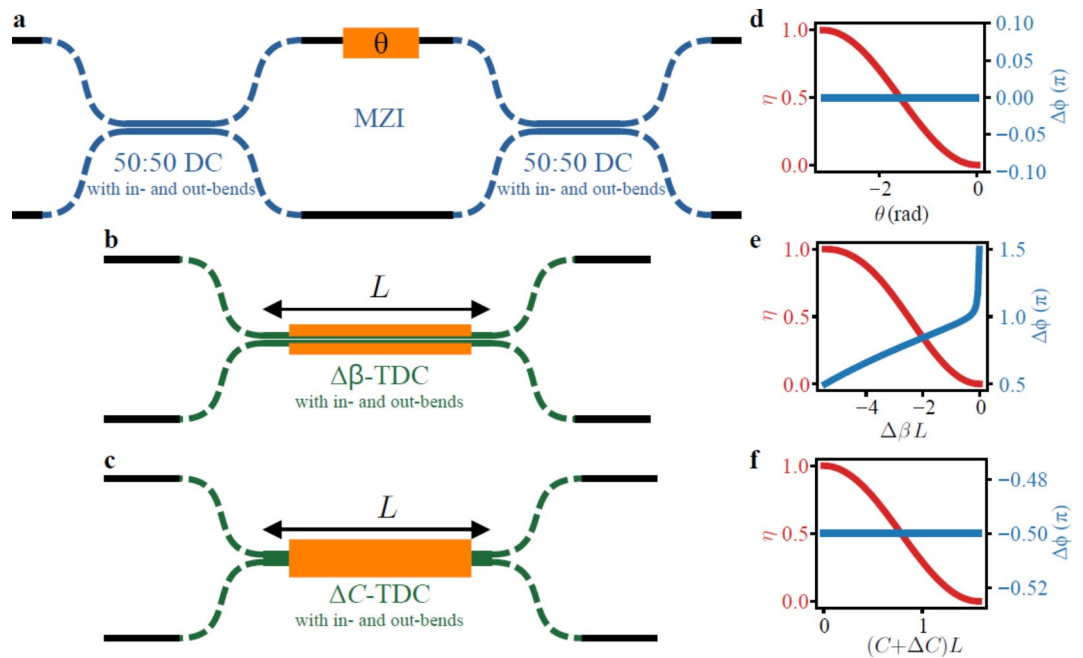


Fig. 1. Fundamental reflectivity-tuning devices and their phase-reflectivity dependence. **(a)** An MZI with a tunable phase shift θ . **(b)** A conventional $\Delta\beta$ -TDC with a coupling length L , controlled by propagation constant tuners. **(c)** The proposed ΔC -TDC with a coupling length L , controlled by a coupling coefficient tuner. The numerical simulation of the reflectivity η (red curve) and relative phase between the optical paths $\Delta\phi$ (blue curve) for the MZI. (This work.) **(d)**, the $\Delta\beta$ -TDC **(e)**, and the ΔC -TDC **(f)**. The relative phase shift is constant in the tunable range only for the MZI and the proposed ΔC -TDC, providing an advantage over the $\Delta\beta$ -TDC for phase-sensitive applications. (Numerical simulation details can be found in the [supplementary materials](#).)

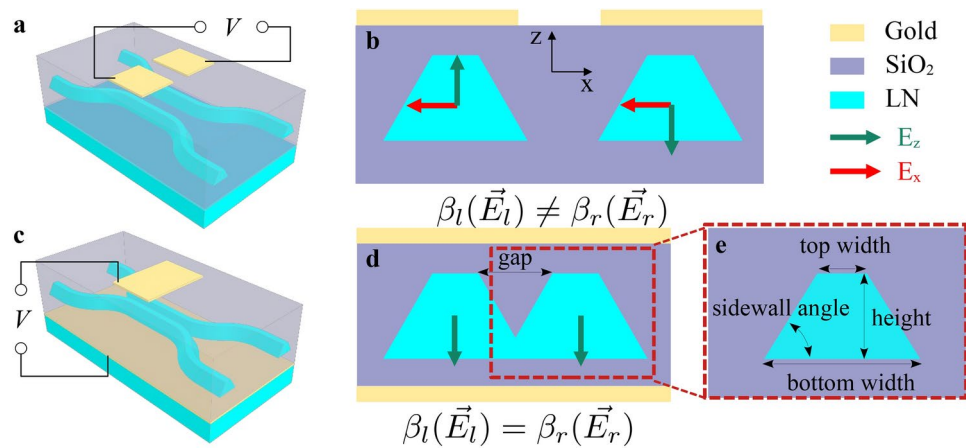


Fig. 2. Z-cut TFLN TDC schematics. **(a)** A schematic of a conventional $\Delta\beta$ -TDC example. **(b)** The cross-section of the $\Delta\beta$ -TDC is shown in **(a)**. The inset coordinate indicates the LN crystal orientation. Green and red arrows indicate the electric field direction at the center of each waveguide when a voltage is applied. By applying a voltage to the right electrode, the left and right waveguides experience the electric field in a different direction (\vec{E}_l and \vec{E}_r), creating a difference between the propagation constants of the left and right waveguides is created ($\Delta\beta = |\beta_l(\vec{E}_l) - \beta_r(\vec{E}_r)|$). Propagation with different propagation constants enables tunability and leads directly to a buildup of a relative phase. **(c)** Proposed ΔC -TDC schematics (optimized geometry parameters are reported in Fig. 4). **(d)** The cross-section of the coupled region. The green arrow indicates the electric field direction at the center of each waveguide when a voltage is applied to the top electrode. Because both the left and right waveguides experience the same electric field, no propagation constant difference between the left and right waveguides is introduced ($\Delta\beta = |\beta_l(\vec{E}_l) - \beta_r(\vec{E}_r)| = 0$). **(e)** Cross-sectional view and descriptive parameters of an individual waveguide within the coupler structure.

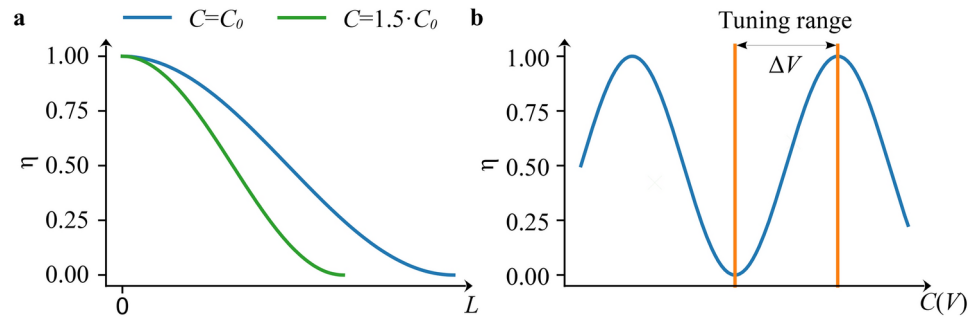


Fig. 3. ΔC -TDC tuning principle. (a) Reflectivity curves of DCs with different coupling coefficients along the propagation of the coupled region (C_0 is an arbitrary value). (b) Output reflectivity change of a ΔC -TDC, which is achieved by controlling the coupling coefficient electro-optically. ΔV as indicated corresponds to a 0 to 1 transition, to which we refer as V_π when the chip length L is given.

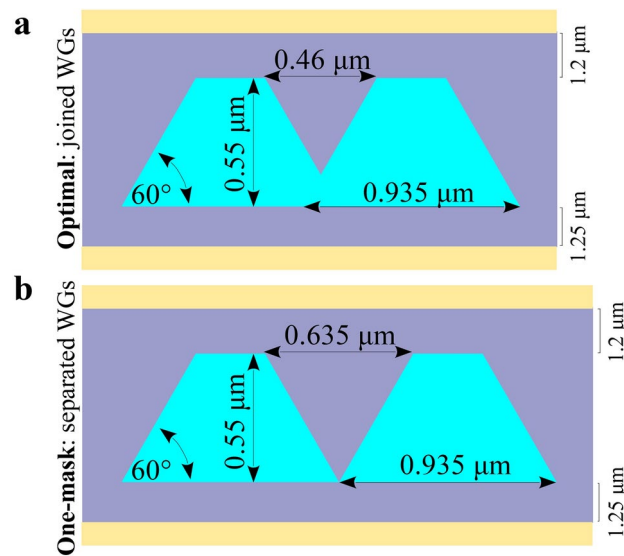


Fig. 4. Geometry parameters of proposed TFLN-based ΔC -TDCs. (a) The geometry with optimal FOM. (b) The optimal geometry allowing for one-mask fabrication.

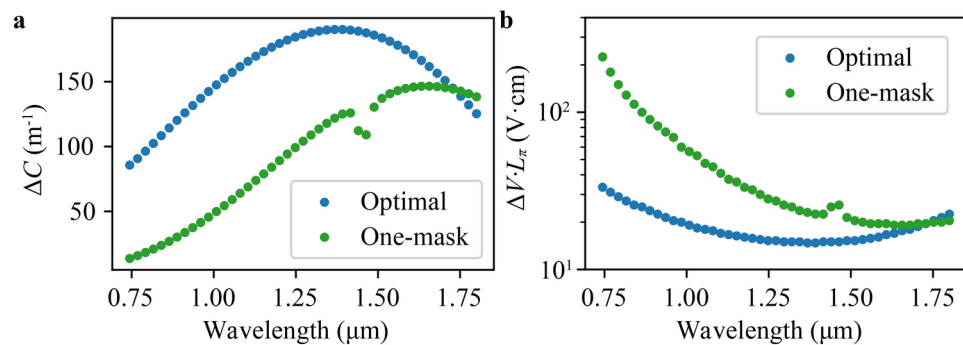


Fig. 5. Tunability of the two proposed ΔC -TDCs. (a) Coupling coefficient variation ΔC induced by $\Delta V = 18 \text{ V}$. (b) Tunability FOM at different wavelengths. At wavelengths of $1.4 \mu\text{m}$ and $1.6 \mu\text{m}$, the optimal and one mask designs, respectively, require the least resources (the out-of-order data points around $1.45 \mu\text{m}$ in the plots for one-mask design are the results of hybridization between the fundamental odd TE mode and fundamental even TM mode, which is expected to affect the coupling behavior at this wavelength).

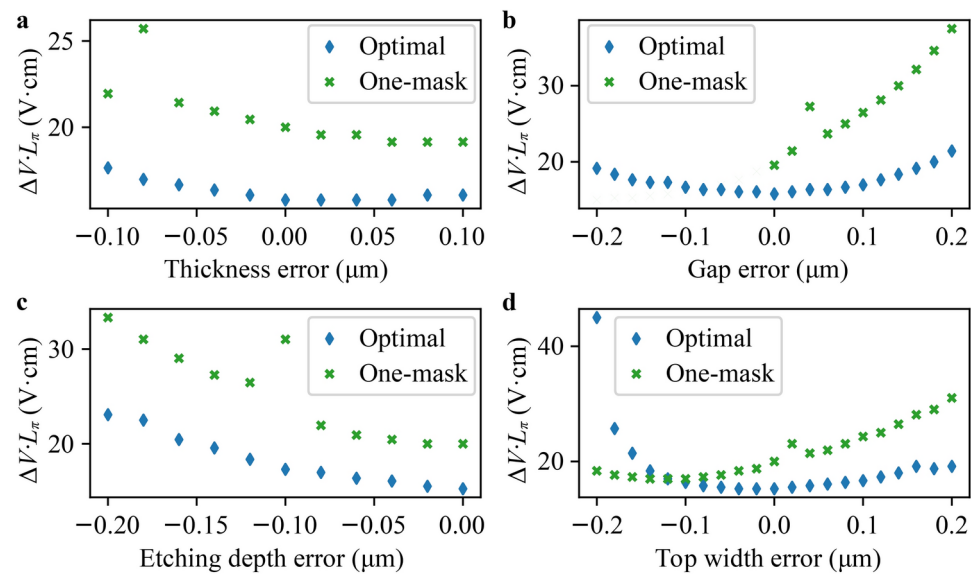


Fig. 6. Fabrication error analysis at 1.55 μm wavelength. (a) Tunability FOM plot for thin film thickness error. (b) Tunability FOM plot for thin gap distance error. (c) Tunability FOM plot for etching depth error. (d) Tunability FOM plot for waveguide top width error.

Device	MZI	$\Delta\beta$ -DC	ΔC -DC
Fab-error robustness	No	No	Yes
Operation bandwidth	N.A. ^a	N.A. ^a	Wide
Phase conservation	Yes	No	Yes
Modulation efficiency @1.55 μm (V·cm)	1.8-3.1	1.8-3.1	15.7
Number of bending section	4	2	2

Table 1. Comparison of fundamental reflectivity tuning devices. (^a MZI and $\Delta\beta$ -DC can only operate at specific wavelengths in a periodic manner that allow them to achieve full 0-1 reflectivity, whereas ΔC -DCs have continuous wide operational wavelength bandwidth.).

phase between coupled waveguides fixed (Fig. 1e, f) and is significantly less sensitive to coupling length and operating wavelength. Moreover, our design eliminates the issue of non-even responses from controllers in the dual-drive design^{26,27}, ensuring consistent and reliable performance over an extra-wide range of wavelengths.

Results and methods
Geometry design

Our design is based on the thin film Lithium Niobate TFLN platform, which is poised to become a material choice for applications relying on the electro-optic (EO) effect, offering significant potential in various applications^{3,28} and enabling ultra-low loss waveguides²⁹. However, this design concept can be applied to any thin film EO materials, including Barium titanate^{30,31}.

Figure 2c shows the schematic of the proposed ΔC -TDC based on Z-cut TFLN. Figure 2d, e present its cross-section of the coupled region and single waveguide, respectively. The TDC consists of two waveguides placed close to each other, allowing for optical power transfer via their evanescent field.

A ΔC -TDC exhibits tunability due to the variation of the coupling coefficient in the coupled region (Fig. 3a, b) while ensuring that the odd mode is perfectly antisymmetric and the even mode perfectly symmetric, thereby resulting in equal propagation constants for both waveguides²⁰. To achieve this uniformity in propagation constants, it is imperative to maintain identical refractive index profiles for the coupled waveguides.

In order to utilize the strongest EO coefficient of LN while preserving uniformity in refractive index profiles, electrodes are placed on the bottom and top of the coupled region of the TDC. Both electrodes are much wider than the total width of the waveguides, generating a homogeneous electric field across two waveguides in the coupled region solely along the z direction.

The relationship between the refractive index and the applied electric field in LN is expressed as:

$$\Delta(1/n^2)_{ij} = \sum_k r_{ijk} E_k \tag{1}$$

where $\Delta(1/n^2)_{ij}$ is the change of the relative permittivity tensor, E_k is the electric field vector, and r_{ijk} is the EO tensor with i, j, k corresponding to x, y, z crystal coordinate. The tensor r_{ijk} can further be expressed using two indices $r_{I,k}$ due to the symmetry property of LN as^{3,32}:

$$r_{Ik} = \begin{pmatrix} 0 & -r_{22} & r_{13} \\ 0 & r_{22} & r_{13} \\ 0 & 0 & r_{33} \\ 0 & r_{42} & 0 \\ r_{42} & 0 & 0 \\ -r_{22} & 0 & 0 \end{pmatrix} \text{ with } I = \begin{cases} 1, & ij = xx \\ 2, & ij = yy \\ 3, & ij = zz \\ 4, & ij = yz, zy \\ 5, & ij = xz, zx \\ 6, & ij = xy, yx \end{cases} \quad (2)$$

where $r_{13} \approx 9.6 \text{ pm/V}$, $r_{33} \approx 30.9 \text{ pm/V}$ ³³.

The change of the refractive index is given by the electro-optic effect (Eqs. 1 and 2), approximately $\Delta n_x \approx -1/2n_o^3 r_{13} E_z$, $\Delta n_y \approx -1/2n_o^3 r_{13} E_z$, $\Delta n_z \approx -1/2n_e^3 r_{33} E_z$ based on first order Taylor expansion³. Subscripts *o/e* stand for ordinary/extraordinary axis and the electric field across the two electrodes along z direction is determined by COMSOL simulations.

Performance optimization

In this section, we describe the details of optimizing the tunability performance of the proposed TDC design.

The TFLN refractive index is based on the Sellmeier equation (see [supplementary materials](#)) provided by Nanoln, which is in line with our previously fabricated devices^{28,29,34,35}. We solve optical modes³⁶ based on the electric-field-dependent (generated by voltage in a range $V \in \Delta V$) refractive index profile to calculate the effective refractive indices of the symmetric and the antisymmetric modes $N_s(V, \lambda)$ and $N_a(V, \lambda)$. The crossover length is calculated as

$$L_c(V, \lambda) = \frac{\lambda}{2(N_s(V, \lambda) - N_a(V, \lambda))} \quad (3)$$

Where λ is the wavelength of the operating light. The coupling coefficient is given by

$$C(V, \lambda) = \frac{\pi}{2 \cdot L_c(V, \lambda)}. \quad (4)$$

We construct a 2×2 Hamiltonian $H(V, \lambda)$ for the TDC by applying continuous quantum walk model for DCs^{37,38}

$$H(V, \lambda) = \begin{pmatrix} \beta_l(V, \lambda) & C(V, \lambda) \\ C(V, \lambda) & \beta_r(V, \lambda) \end{pmatrix} \quad (5)$$

where the waveguide propagation constants are assumed to be identical with their values derived from the supermodes $\beta_l(V, \lambda) = \beta_r(V, \lambda)$ ³⁹.

The unitary transformation implemented by the ΔC -TDC is given by the time evolution of the Hamiltonian $H(V, \lambda)$ over the effective coupled length L

$$U(V, \lambda, L) = e^{-iH(V, \lambda)L}. \quad (6)$$

The unitary transformation implemented by a DC can be written in the form of⁴⁰.

$$U(V, \lambda, L) = \begin{pmatrix} \sqrt{\eta(V, \lambda, L)} & i\sqrt{1-\eta(V, \lambda, L)} \\ i\sqrt{1-\eta(V, \lambda, L)} & \sqrt{\eta(V, \lambda, L)} \end{pmatrix} \quad (7)$$

where $\eta(V, \lambda, L)$ is the reflectivity. Accordingly, the reflectivity is given by

$$\eta(V, \lambda, L) = |U_{11}(V, \lambda, L)|^2. \quad (8)$$

We define L_π as the minimum length that the TDC needs to implement a 0 – 1 full reflectivity change within the range ΔV for a given wavelength λ . The requirement is then that $L_\pi C(V)$ covers the full range between $k\pi$ and $(k + \frac{1}{2})\pi$ or alternatively between $(k + \frac{1}{2})\pi$ and $(k + 1)\pi$, for some $k \in \mathbb{Z}$. (Details can be found in the [supplementary materials](#)).

To determine the tunability performance of a ΔC -TDC, we define as the figure of merit (FOM) for the tunability of a ΔC -TDC:

$$\text{FOM}(\lambda) = \Delta V \cdot L_\pi \quad (9)$$

with a unit of $V \cdot \text{cm}$. The FOM indicates the resources of voltage range and coupling length required to achieve 0-to-1 reflectivity. Accordingly, it pinpoints an optimal combination in terms of the resources coupling length L_π and voltage range ΔV . This concept is similar to $V_\pi \cdot L$ in modulators, which indicates device size and modulation efficiency. We use $\Delta V \cdot L_\pi$ to characterize ΔC -TDCs, as their tuning principle differs.

Proposed devices

In this section, we present simulation results for the proposed ΔC -TDCs. The first coupler design corresponds to the fully optimized structure, which has a small waveguide gap of $0.46 \mu\text{m}$ (FOM=15.7 $V \cdot \text{cm}$ at wavelength $1.55 \mu\text{m}$) as shown in Fig. 4a and requires two iterations of electron beam lithography (EBL) and etching. To simplify the fabrication process, we also provide the results for the second design, featuring a gap of $0.635 \mu\text{m}$ (FOM=19.5 $V \cdot \text{cm}$ at wavelength $1.55 \mu\text{m}$) as shown in Fig. 4b, which requires a single EBL and etching iteration. The modes and propagation simulations of the two coupler designs are reported in the [supplementary materials](#).

In the optimization process^{41,42}, we minimize the FOM of the ΔC -TDC. We set the simulation in a voltage range $\Delta V = 18 \text{ V}$ (a random but realistic value) at a wavelength of $1.55 \mu\text{m}$ and distance between the top and bottom thin film gold⁴³ electrodes $1.5 \mu\text{m}$. The electrodes need to be placed with a minimum gap of $1 \mu\text{m}$ between waveguides to avoid optical losses due to absorption caused by electrodes. The parameters we optimized are thin film thickness, etching depth, waveguide top width, gap distance between the top of two waveguides, and sidewall angle in the range of $[0.3, 0.9] \mu\text{m}$, $[0.1, 0.9] \mu\text{m}$, $[0.1, 2.2] \mu\text{m}$, $[0.1, 1.2] \mu\text{m}$, and $[45^\circ, 75^\circ]$ respectively.

The tunability depends on the relative magnitude of the static coupling coefficient and the variation of the coupling coefficient introduced within ΔV . A greater static coupling coefficient requires a shorter coupled length to achieve the same tunability given by a fixed ΔC . We report the variation of coupling coefficients of the two ΔC -TDCs in the voltage range ΔV at different wavelengths in Fig. 5a. When $C \gg \Delta C$, the tunability can be considered as solely given by the variation in coupling coefficient within ΔV .

Additionally, when the gap between two waveguides becomes very small, it is necessary to consider the effects of higher-order modes, including radiation modes, as they can introduce losses and limit the efficiency of power transfer. However, our waveguide structure is designed to support only the propagation of fundamental modes (single-mode waveguide), and the gap is not small enough for the two waveguides to behave as a single waveguide. Therefore, the impact of higher-order modes on the overall power transfer ratio is negligible for our designs, which is verified in 3D Finite-difference time-domain (FDTD) simulations, as shown in the [supplementary materials](#).

We report the FOM of tunability of the two proposed ΔC -TDCs in Fig. 5b. The FOM of the optimal design can achieve $15 V \cdot \text{cm}$ across wavelength from 1.25 to $1.58 \mu\text{m}$ and the FOM of the one-mask design is below $20.5 V \cdot \text{cm}$ across wavelength from 1.45 to $1.8 \mu\text{m}$. The operation wavelength bandwidth is continuous and much broader than MZIs and $\Delta\beta$ -TDCs. The optimal design achieves its best FOM at a wavelength of approximately $1.368 \mu\text{m}$, with a 3-dB bandwidth (defined as the operational spectrum range achieving an FOM within less than a 50% increase from its peak FOM at a given wavelength) ranging from $0.912 \mu\text{m}$ to $1.776 \mu\text{m}$. The one-mask design achieves its best FOM at a wavelength of around $1.632 \mu\text{m}$, with its 3-dB bandwidth starting at $1.248 \mu\text{m}$.

For comparison, conventional $\Delta\beta$ -TDCs, fabricated with titanium-diffused bulky LN technology, typically operate at switching voltages below 10 V but with a device length longer than 1 cm ²¹. Furthermore, MZI modulators and $\Delta\beta$ -TDC in which two waveguides experience electric fields in an opposite direction require less driving or electrode length to achieve π phase change, particularly in x-cut LN²⁴. Specifically, MZI modulators based on x-cut TFLN achieve $V_\pi \cdot L$ values of 1.8 – 3.1 V cm in a monolithic manner^{44–46}, and 2.1 – 3 V cm in a hybrid manner^{47–49} respectively. Additionally, $V_\pi \cdot L$ value of 7.4 V cm has been demonstrated in z-cut TFLN with one arm modulation⁵⁰.

Fabrication error analysis

TFLN is a relatively new technology, and accordingly, the fabrication process is somewhat immature³. We analyze how fabrication errors affect the tunability of our couplers with respect to film thickness, gap distance, etching depth, and waveguide top width at a wavelength of $1.55 \mu\text{m}$ as shown in Fig. 6a–d respectively, with a fixed 60° sidewall angle. The sidewall angle is given by the chemistry settings of the etching process and can be kept constant. We postulate a uniform fabrication quality across both waveguides within the coupler structure while addressing individual error sources sequentially. The simulation results indicate that a $\sim 100 \text{ nm}$ fabrication error does not significantly affect the tunability and larger errors ($\sim 200 \text{ nm}$) can be compensated by increasing the coupler length or operating voltage range.

In addition to symmetric fabrication errors discussed above, asymmetric fabrication errors may also occur in practice. Such errors can result in dimensional differences between waveguides, preventing the device from achieving 0-1/1-0 reflectivity due to phase mismatches²⁰. This challenge can be mitigated by improving fabrication quality or by introducing additional tuners to locally adjust the propagation constants of individual waveguides, similar to the dual-drive design²⁷. This approach can be feasible in electro-optic devices, as electro-optic effects offer precise control over local parameters^{8,51}.

Discussion

In this paper, we proposed a design of a TDC with optimized geometries in the Z-cut TFLN platform. It allows arbitrary splitting ratio tuning while ensuring a common phase between waveguides across an extra-wide range of operating wavelengths. Furthermore, it exhibits intrinsic robustness to fabrication errors.

Several crucial aspects need to be considered when comparing the design of the three fundamental reflectivity-tuning devices. A summarized comparison of fundamental tuning devices is presented in Table 1. In terms of fabrication error, MZIs are well-known for being sensitive because of the requirement of perfect balanced

directional couplers to achieve a full 0-1 reflectivity. Additionally, directional couplers are designed for specific operating wavelengths, rendering MZIs wavelength-dependent devices. On the other hand, $\Delta\beta$ -TDCs have to be designed to present 0 reflectivity when static to ensure a complete 0-1/1-0 reflectivity, which makes such devices wavelength-dependent and less resilient to fabrication errors. On the contrary, ΔC -TDCs can achieve a complete 0-1/1-0 reflectivity in a wide range of wavelengths and have shown robustness to fabrication error in simulations. Regarding the independent phase control required in applications such as quantum information processing, all three devices need an extra phase shifter. MZIs and ΔC -TDCs can maintain a constant phase when working as reflectivity tuning devices, resulting in straightforward phase control. However, the phase of a $\Delta\beta$ -TDC changes while its reflectivity is tuned and requires device-dependent characterization, which is challenging in practice. As for the driving voltage, ΔC -TDCs require higher amplitudes compared to MZIs and $\Delta\beta$ -TDCs when considering the same device size given the state-of-the-art technologies^{21,45}. This is because propagation constants tuning is more efficient for MZIs and $\Delta\beta$ -TDCs. However, the driving voltage for ΔC -TDCs can be reduced by increasing the length of the coupled region. Alternatively, the figure of merit (FOM) can be improved by decreasing the gap between electrodes or by utilizing materials with stronger electro-optic effects, potentially in a hybrid fashion⁵². Finally, in terms of the number of required bending sections, an MZI needs two more sections than both types of TDCs. This causes more losses, which becomes problematic when cascading multiple stages of MZIs^{22,53,54}. Such cascading designs aim to overcome the challenges associated with the need for ideal balanced DCs in the MZIs. TDCs require fewer bendings, which makes them potentially experience less photon loss in large-scale circuits¹¹⁻¹³. However, they may need to be designed longer to compensate for fabrication errors and high driving voltage requirements.

In addition to Z-cut TFLN, our design can be implemented with X-cut TFLN, although more challenging. This is due to the requirements of the electrode positioning⁵⁵ and the need for a small waveguide geometry that can only be realized with cutting-edge thin film technology. While nanofabrication technology in LNOI has facilitated the development of numerous wafer-scale devices, it may not be sufficient to meet the requirements for such devices. Moreover, based on state-of-the-art studies^{10,17,22,23,29}, it is reasonable to assume that each bending section contributes at least 0.1 dB loss. Additionally, TFLN waveguides with polished surface roughness have demonstrated propagation loss as low as 0.027 dB/cm⁵⁶. Given that the ΔC -TDC has one fewer bending section, a device no longer than approximately 3.7 cm with polished waveguides would have a loss advantage over MZIs that contain two bending sections. Enhancing sidewall roughness as well as designing efficient mode size converters are required, as these improvements will contribute to minimizing optical losses due to the small patterning features and ensuring the practical viability of the proposed device.

Our design concept is versatile and can be applied to any thin film EO materials, including Barium titanate^{30,31}. As for the silicon platform, which is currently very popular in building PICs, our design can also be applied with thermal-optic devices. In contrast to electro-optic devices, thermo-optic devices do not offer the capability of cryogenic temperature operation⁵⁷ and high-speed reconfiguration⁴⁵. To avoid thermal crosstalk, waveguides on thermal-optic circuits need to be spaced at a distance even with more advanced fabrication technology^{58,59}. Meanwhile, electro-optic devices need less space in the vertical direction relative to the light propagation with lower power consumption⁸. Alternatively, the plasma dispersion effect is extensively employed for high-speed phase modulation⁶⁰. However, devices utilizing this effect experience greater optical losses with increased tuning efficiency⁶¹. This is non-ideal for applications that are sensitive to optical losses, including building large-scale photonic circuits.

Lastly, the proposed ΔC -TDC device is suitable for applications that are insensitive to high driving voltage but require maintaining a fixed relative phase. Moreover, such devices may be used as a tunable wavelength multiplexer-demultiplexer⁶² or be cascaded to enhance filtering performance due to its wavelength-reflectivity-dependent operation. Additionally, ΔC -TDCs could expand the functionalities of field-programmable photonic arrays and find applications in self-calibrating programmable PICs^{27,63-66}.

Data availability

All data generated or analysed during this study are included in this published article and its supplementary information files.

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Author contributions

Y.Y. conceived and designed the device. Y.Y. and H.H. carried out the simulations. Y.Y., T.W., A.K., and A.P. prepared the manuscript. Y.Y., T.W., A.K., and A.P. analyzed the data and discussed the results. A.P. directed the project.

Declarations

Competing interests

The authors declare no competing interests.

Additional information

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