

## “Green” use of fluorocarbons in Cherenkov detectors and silicon tracker cooling systems: challenges and opportunities

Gregory Hallewell<sup>a,\*</sup>

<sup>a</sup>Aix Marseille Université, CNRS/IN2P3, CPPM, Marseille, France

E-mail: [greggh@cppm.in2p3.fr](mailto:greggh@cppm.in2p3.fr), [gregory.hallewell@cern.ch](mailto:gregory.hallewell@cern.ch)

Saturated fluorocarbons (SFCs: chemical form  $C_nF_{(2n+2)}$ ) are chosen for their optical properties as Cherenkov radiators, with  $C_4F_{10}$  and  $CF_4$  used in the COMPASS and LHCb Ring Imaging Cherenkov detectors at CERN. Their non-conductivity, non-flammability and radiation resistance also make them ideal coolants, with  $C_6F_{14}$  liquid used in all LHC experiments, and  $C_3F_8$  used as an evaporative coolant in the ATLAS silicon tracker. While SFCs have high Global Warming Potentials (GWP typically  $> 5000 \cdot CO_2$ ), fluoro-ketones (FKs: of chemical form  $C_nF_{2n}O$ ) can offer similar performance at very low, or zero-GWP.

This paper considers use of heavy SFC and FK vapours in Cherenkov detectors. The blending of high-order ( $C > 4$ ) SFC or FK vapours with a light carrier gas is explored to replicate the refractivities of  $CF_4$  and  $C_4F_{10}$ , to reduce or eliminate the GWP “load” (in equivalent tonnes of  $CO_2$ ) in large Cherenkov radiator volumes. Subject to optical testing, 3M NOVEC<sup>®</sup> 5110 ( $C_5F_{10}O$ ) - blended with  $N_2$  and controlled in real time using sound velocity gas mixture analysis - could replace  $C_4F_{10}$  and  $CF_4$  in RICH detectors. New, non-cyclic isomers of  $C_4F_8O$  could directly replace  $C_4F_{10}$  and - blended with  $N_2$  - also replace  $CF_4$ .

Noting the impending EU restrictions on fluorinated compounds, and (2025) withdrawal of 3M Corp. from the PFAS (Per- and poly-fluoroalkyl substances) market, radiator GWP load reduction through use of legacy stocks of  $C_5F_{12}$  &  $C_4F_{10}$  - blended with  $N_2$  to replicate the respective refractivities of  $C_4F_{10}$  &  $CF_4$  - is also considered.

The radiation tolerance and thermal performance of 3M NOVEC<sup>®</sup> 649 ( $C_6F_{12}O$ ) liquid was sufficiently promising for to be considered to replace  $C_6F_{14}$  in liquid cooling applications at CERN. Although not industrialized over the full  $C_nF_{2n}O$  range, lighter ( $C < 4$ ) fluoro-ketone molecules - for example  $C_2F_4O$  isomers, with similar thermodynamics to  $C_2F_6$ , and subject to toxicity, materials compatibility and low-GWP verifications - might allow lower operating temperatures than possible with evaporative  $C_3F_8$  or  $CO_2$  for the cooling of future silicon trackers operating in high luminosity environments.

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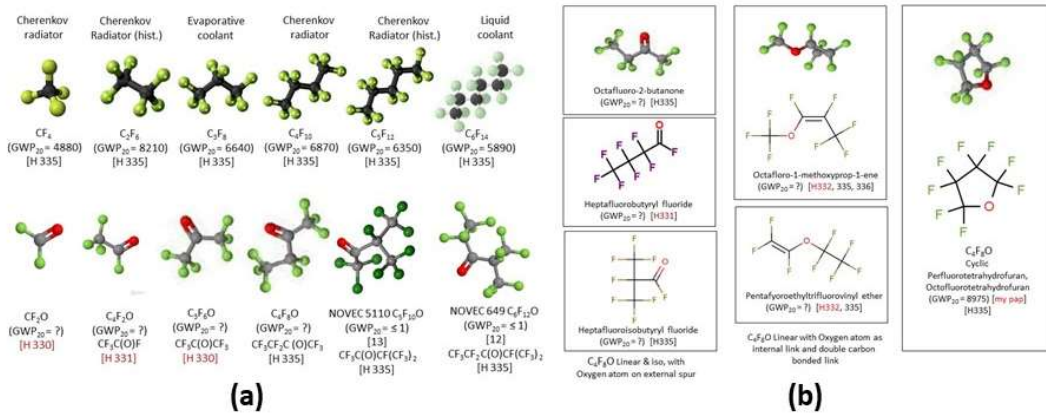
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## 1. Introduction

Saturated fluorocarbons (SFCs: of chemical structure  $C_nF_{(2n+2)}$ ) are chosen for their optical properties as Ring Imaging Cherenkov detector radiators. At CERN LHCb RICH-2 uses a 100 m<sup>3</sup> CF<sub>4</sub> radiator, while COMPASS and LHCb RICH-1 respectively use 100 m<sup>3</sup> & 4 m<sup>3</sup> of C<sub>4</sub>F<sub>10</sub>.

SFCs are non-toxic, non-ozone-depleting, radiation resistant, non-conductive and non-flammable, making them ideal coolants for electronics and semiconductor trackers. However their high Global Warming Potentials (GWPs 5000-9000\*CO<sub>2</sub>) contributed 37% to CERN’s CO<sub>2</sub> and CO<sub>2</sub>-equivalent direct emissions in 2022 [1], for an SFC loss of around 10 tonnes. Partly through reduced SFC use and losses, improved monitoring and closed-circulation [2], CERN aims by the end of 2025 to reduce its CO<sub>2</sub> equivalent emissions to 72% of 2018 levels.

Figure 1a illustrates the molecular shapes of common SFCs, along with their 20-year GWPs and (low) inhalation toxicity ratings ([H335] under the GHS classification scheme [3]). Below are shown their same carbon-order fluoro-ketone (FK) analogues, based on non-cyclic, spurred oxygen  $C_nF_{2n}O$  molecular topology.



**Figure 1a:** *upper row:* molecular shapes of SFCs, including Cherenkov gas radiators and coolants  
*lower row:* shapes of non-cyclic  $C_nF_{2n}O$  FK analogues.  
 20-year GWPs and GHS hazard ratings [3] shown where known or listed.  
**Figure 1b:** Shape examples of cyclic, non-cyclic & non-cyclic, double carbon-bonded  $C_4F_8O$  FK isomers.

Among the FKs octofluoro-tetrahydrofuran (cyclic- $C_4F_8O$ : CAS no. 773-14-8) was studied as a potential Cherenkov gas radiator [4]. Despite offering similar optical performance to  $C_4F_{10}$  its robust closed molecular ring geometry (fig. 1b - *right*), - incorporating the oxygen atom as an internal link - offered no improvement in GWP.

The 3M NOVEC<sup>®</sup> range currently includes two non-cyclic (spurred oxygen)  $C_nF_{2n}O$  molecular forms [5]. NOVEC649 (Perfluoro-2-methyl-3-pentanone, CAS no. 756-13-8:  $C_2F_5C(O)CF(CF_3)_2$ ) and NOVEC5110 (Perfluoro-2-methyl-3-butanone, CAS no. 756-12-7:  $CF_3C(O)CF(CF_3)_2$ ). As with the SFCs, these fluids are non-flammable, non-toxic, non-conductive and non oxone-depleting, but with GWPs of  $\leq 1$ . They are of interest at CERN. The radiation tolerance of NOVEC 649 was tested and looked encouraging [6] for liquid cooling in high radiation zones near the LHC beams. It currently cools multi-anode PMTs in LHCb RICH application [7], but unresolved concerns remain on possible acid formation in the presence of water, and materials compatibility [7].

By analogy with NOVEC 649 & 5110 an attractive candidate Cherenkov radiator gas might be the non-cyclic  $C_4F_8O$  isomer Octafluoro-2-butanone (CAS no. 337-20-2:  $CF_3CF_2C(O)CF_3$ ). Several  $C_4F_8O$  FK isomers are shown in fig. 1b. It is likely that geometries with the oxygen atom on a spur of the molecule will have low GWPs, as in the case of NOVEC5110. Isomers having the oxygen atom at the end of the molecule tend to have higher inhalation toxicity, exemplified by GHS hazard ratings H330 and H331 [3]. As the order  $n$  of the  $C_nF_{2n}O$  molecule decreases fewer isomers and oxygen atom placements are available: toxicity ratings are greater at the ‘light’ end of the carbon ‘spectrum’.

While optical and radiation resistance performance might motivate a “special case” argument for continued SFC use at CERN, legislation and external market forces will limit future availability. In 2023 the European Chemical Agency (ECHA) published a list of more than 10 000 per- and poly-fluoroalkyl substances (PFAS) to be investigated for future restriction [8]. The EU aims to reduce, by 2025, the use of fluorinated chemicals to 25% of 2015 levels, partly through application of dynamically-varying levies [2]. An outcome might be the disappearance of most SFCs and some FKs, conversely perhaps with the industrialisation of new low-GWP alternatives. Future industrialization of safe  $C_nF_{2n}O$  substitutes for SFCs will probably be dominated by the needs of semiconductor manufacture, vapour phase reflux soldering and cooling in the electronics industry.

## 2. GWP reduction in Cherenkov gas radiators: motivation and methodology

A Cherenkov radiator of volume  $V(m^3)$  containing gases of densities  $\rho_i (kgm^{-3})$ , molar concentrations  $w_i$  and individual Global Warming Potentials  $GWP_i$  can be considered to have a GWP environmental “load” (and release potential)  $L$  (in tonnes  $CO_2$  equivalent) given by:

$$L = \frac{V}{1000} \sum_i \omega_i \cdot \rho_i \cdot GWP_i \quad (1)$$

The refractivity of the radiator gas mixture,  $(n-1)_{rad}$ , can be calculated according to:

$$(n-1)_{rad} = \sum_i \omega_i (n-1)_i \quad (2)$$

The GWP load,  $L$ , can be reduced by blending a heavier vapour,  $x$ , of refractivity  $(n-1)_x$  at low molar concentration,  $\omega_x$ , with a light gas,  $y$ , of refractivity  $(n-1)_y$  to replicate the refractivity  $((n-1)_{ztarget})$  of a lighter SFC,  $z$ , being replaced:

$$w_x = \frac{((n-1)_{ztarget} - (n-1)_y)}{((n-1)_x - (n-1)_y)} \quad (3)$$

Ideally the heavier component would be a zero-GWP FK, but the use of legacy stocks of  $C_4F_{10}$  and  $C_5F_{12}$  could also result in significant GWP load reductions, particularly in the large COMPASS and LHCb RICH-2 radiators.

A Cherenkov radiator often contains small molar concentrations of light contaminant gases including  $CO_2$  and  $O_2$ , whose concentrations can be respectively monitored by Non-Dispersive Infra-Red (NDIR) sensors and electrochemical cells. For a group of up to  $j_{max}$  contaminant gases of individual molar concentrations  $w_j$  and refractivities  $(n-1)_j$  eq. (3) can be recast as:

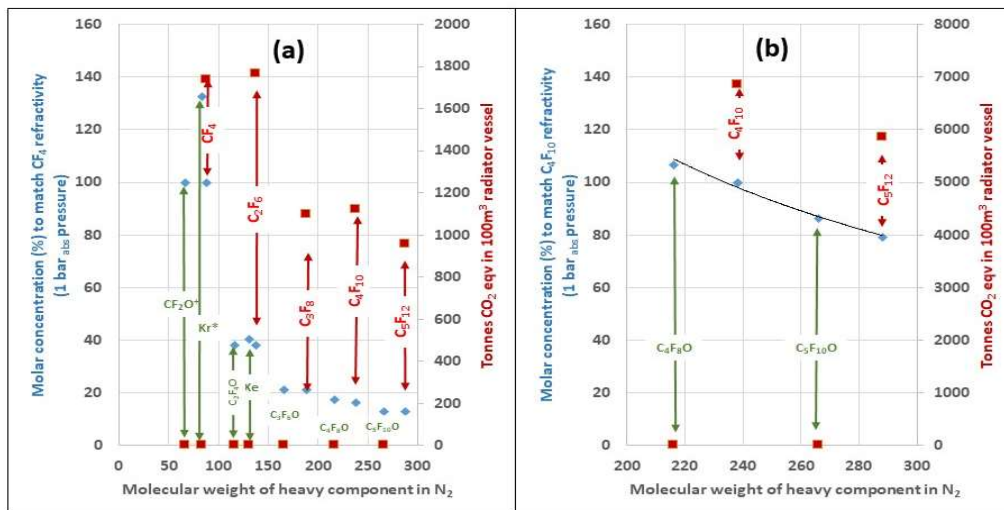
$$w_x = \frac{(n-1)_{ztarget} - (n-1)_y - \sum_{j=1}^{j_{max}} w_j [(n-1)_j - (n-1)_y]}{(n-1)_x - (n-1)_y} \quad (4)$$

while eq. (2) becomes:

$$(n-1)_{z(target)} = w_x [(n-1)_x - (n-1)_y] + (n-1)_y + \sum_{j=1}^{j_{max}} w_j [(n-1)_j - (n-1)_y] \quad (5)$$

Figure 2 illustrates the GWP load in  $100m^3$  radiator volumes at operating pressure of  $10^5$  hPa (1 bar<sub>abs</sub>) as the refractivity of (a)  $CF_4$  ( $(n-1)_z=488.10^{-6}$ ,  $L_{100m^3}=1737$  t) and (b)  $C_4F_{10}$  ( $(n-1)_z=1450.10^{-6}$ ,  $L_{100m^3}=6849$  t) are respectively replicated by blends of a heavier SFC or FK gas in a light zero-GWP carrier (for example  $N_2$  :  $(n-1)_y = 310.10^{-6}$ ). A load reduction of 44.9% ( $1737 \rightarrow 957$ t) is seen using  $C_5F_{12}$  ( $(n-1)_z=1750.10^{-6}$ ) at 13% molar concentration, and 35.6% ( $1737 \rightarrow 1119$ t) with  $C_4F_{10}$  ( $(n-1)_z=1450.10^{-6}$ ) at 16.3%. Reductions using  $C_2F_6$  and  $C_3F_8$  would be less, due to the higher molar concentrations required, with none in the case of  $C_2F_6$  due to its higher GWP. Load reductions through the replacement of  $CF_4$  with around 14% of NOVEC5110  $C_5F_{10}O$  FK would be total, as also for a suitable non-cyclic  $C_4F_8O$  isomer blended at around 18%. Here unknown FK refractivities have been assumed the same as the corresponding SFCs; a probable overestimate since they are lighter by 22 units of molecular weight. Their required concentrations can thus be expected to be slightly higher. For ‘completeness’, hypothetical blend concentrations are also shown for several lower-order FKs, including  $C_3F_6O$  and  $C_2F_4O$ , although these would probably be toxicologically unsuitable (fig. 1a). Substitutions with xenon and krypton are

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**Figure 2b:** refractivity of  $C_4F_{10}$  replicated by blends of a heavier m.w. vapour in a nitrogen carrier.

**Figure 2b:** refractivity of  $C_4F_{10}$  replicated by blends of a heavier m.w. vapour in a nitrogen carrier.

For C<sub>4</sub>F<sub>10</sub> replacement there is clearly less room to manoeuvre; the only practical high-order alternatives are C<sub>5</sub>F<sub>12</sub> or NOVEC5110. (Substitution with C<sub>4</sub>F<sub>8</sub>O would probably require a slight overpressure due to its higher density.) A reduction in GWP load of 14.5% can be expected with C<sub>5</sub>F<sub>12</sub> at 79% concentration (6849→5857) and the GWP load reduction with NOVEC5110 at around 85% molar concentration is total, of course. Since the boiling points of C<sub>5</sub>F<sub>12</sub> and NOVEC5110 at atmospheric pressure are respectively 30 and 27 °C it may be necessary to warm the outer surface of the Cherenkov radiator vessel above this temperature if high concentrations of these fluids are used. Since the refractivities of non-cyclic FKs are currently unknown, Figs 2a & 2b are only an indicator of what may be achievable, but might stimulate optical measurements in these fluids.

### 3. Blending and the blend monitoring approach

Sound velocity,  $v_s$ , is continuously monitored to determine the concentrations,  $w_{i=1,2}$ , of a pair of gases of primary interest (in ATLAS:  $C_3F_8$  into  $N_2$ -purged environmental volumes) in the presence of known concentrations of other contaminant gases [9]:

$$v_s = \sqrt{\frac{\frac{\sum_i \omega_i C_{P_i}}{\sum_i \omega_i C_{V_i}} \cdot R \cdot T}{\sum_i \omega_i M_i}} \quad (6)$$

where  $M_i$ ,  $C_{p,i}$  and  $C_{v,i}$  are the molecular weights and specific heats at constant pressure and volume for all the gases in the blend,  $R$  is the molar gas constant ( $8.3145 \text{ J} \cdot \text{mol}^{-1} \cdot \text{K}^{-1}$ ), and  $T$  is the absolute temperature (K). The

ATLAS sonar SFC leak monitoring system and algorithm are sensitive to changes in  $C_3F_8$  concentration of  $10^{-5}$  in  $N_2$  on top of varying known concentrations of  $CO_2$ , typically in the range 0-20000 ppm [9].

Figure 3 illustrates sound velocity monitoring of Cherenkov thresholds for particle species. In (a) legacy  $C_4F_{10}$  is considered to replace  $CF_4$  in the context of the LHCb RICH-2 radiator, while in (b)  $C_5F_{12}$  replaces  $C_4F_{10}$  for COMPASS and LHCb RICH-2. Sound velocity in  $C_5F_{12}$  and  $C_4F_{10}$  is based on extensive thermodynamic data: corresponding required concentrations for  $C_5F_{10}O$  and  $C_4F_8O$  will be slightly higher due to their lower densities.

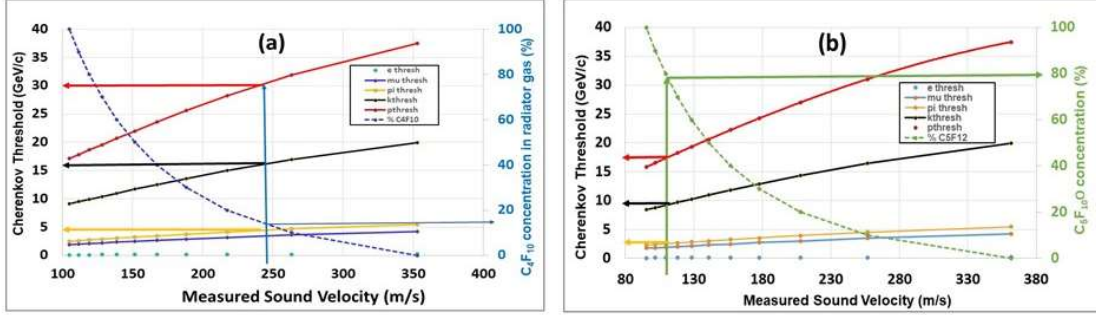


Figure 3: (a) sound velocity monitoring of Cerenkov thresholds: 16 % legacy  $C_4F_{10}$  (in  $N_2$ ) replacing  $CF_4$  (b) with 79 % legacy  $C_5F_{12}$  (in  $N_2$ ) replacing  $C_4F_{10}$ .

#### 4. GWP reduction in the cooling of silicon trackers

Currently  $C_6F_{14}$  is used extensively at CERN as a liquid coolant, including for part of the CMS silicon tracker, while  $C_3F_8$  evaporatively cools part of the ATLAS silicon tracker. Both fluids are to be replaced by evaporative  $CO_2$  cooling in the upgraded CMS and ATLAS trackers, planned for High Luminosity LHC operation (2029-41).  $CO_2$  evaporative cooling has been successfully applied in the upgraded LHCb VELO silicon tracker, evaporating within (200 x 120)  $\mu m$  micro-channels etched into 500  $\mu m$  thick silicon heat sink plates onto which pixel detector modules are bonded. The heat conduction path to the evaporant is very short, with few material interfaces, giving excellent thermal figures of merit ( $TFM$ ) in the range 1.5-3.5  $K \cdot cm^2 \cdot W^{-1}$  [10], where:

$$TFM = \frac{(T_{(Si \text{ module})} - T_{Coolant})}{(Si \text{ module power}/cm^2)} \quad (7)$$

The upgraded CMS and ATLAS silicon trackers will use a ‘tube & block’ construction method with metallic cooling tubes and blocks attaching the silicon modules. Thermal paths are longer, with more material interfaces and correspondingly inferior  $TFMs$ , in the range 24 - 40  $K \cdot cm^2 \cdot W^{-1}$  [11]. Concern has been raised that  $CO_2$  may be unable to maintain silicon modules cold enough for adequate protection against leakage current-induced thermal runaway throughout the full HL-LHC program. It is planned to replace the ATLAS ITk inner pixel layers part way through. This temperature limitation is related to the high  $CO_2$  triple point at  $-56^\circ C$  and the known loss

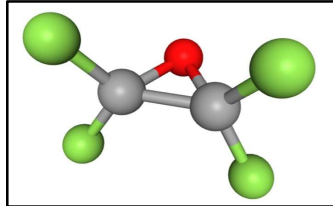


Figure 4: Tetrafluorooxirane  $C_2F_4O$ : a speculative evaporative coolant?

in  $CO_2$  system performance below  $-40^\circ C$  [12]. Maintaining a sufficient safety margin or ‘thermal headroom’ below the expected onset temperature of thermal runaway is more demanding as silicon modules accumulate high

radiation doses during the HL-LHC profile. These concerns have led to the exploration of alternative cooling approaches, including the use of krypton evaporative cooling in a complex transcritical thermodynamic cycle [12]. Fluids with better adapted thermodynamics include xenon and  $C_2F_6$ <sup>1</sup>. The high GWP of  $C_2F_6$  (fig. 1a) is problematic. By analogy with the similar thermophysical characteristics of  $C_6F_{14}$  and  $C_6F_{12}O$  [6], a  $C_2F_4O$  isomer might be worth consideration. While the Trifluoroacetyl fluoride isomer (fig. 1a) has undesirable toxicity, Tetrafluorooxirane (CAS no. 694-17-7; fig. 4) - though a closed ring topology - might be worth investigation through GWP, toxicology, radiation resistance and material compatibility studies.

## 5. Conclusion

This paper has considered use of high GWP  $C_nF_{(2n+2)}$  SFC and  $C_nF_{2n}O$  FK fluids as Cherenkov radiator media and detector coolants in high radiation environments. Ultrasonic blending of high-order ( $C > 4$ ) SFC or FK vapours with light carrier gas could replicate the refractive index of  $CF_4$  and  $C_4F_{10}$ , while reducing or eliminating their GWP “load” (tonnes  $CO_2$  eqv.) in large Cherenkov radiators. In addition to ongoing studies with  $C_6F_{12}O$ , consideration should also be given to study non-cyclic forms of  $C_4F_8O$  and perhaps also the TFO  $C_2F_4O$  isomer, which might offer advantages over  $C_3F_8$  and  $CO_2$  as an evaporative coolant for silicon tracking detectors.

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<sup>1</sup> Critical temperature & pressure for  $C_2F_6$ : 19.8 °C & 30.4 bar<sub>abs</sub>; for Xe: 16.6 °C & 58.4 bar<sub>abs</sub>