

Multichannel switching in a multigap gas switch at atmospheric pressure

A. A. Zherlitsyn[✉] and E. V. Kumpyak

Institute of High Current Electronics, 2/3 Akademicheskoy Avenue, Tomsk, 634055, Russia



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The multichannel switching mode of a controlled multigap switch is studied. The switch is designed for capacitive energy storage, with a charging voltage of up to 100 kV and an energy output time of about 100 ns. The interval between the high-voltage and low-voltage electrodes of this switch is divided into seven series-connected gaps using ball electrodes, and six parallel rows of these ball electrodes allow for multichannel switching. An optical system based on collimators and photodiodes was used to determine the number of channels in the switch gaps. Statistics on the number of channels were collected and the probability of ignition of parallel spark channels was calculated for each of the switch gaps under different operating conditions. We show that both the electrical isolation between the channels and the rate of rise of the triggering pulse significantly affect the number of parallel ignited channels and their distribution over consecutive gaps. At a high triggering voltage pulse rise rate (~ 800 kV/ μ s), a larger number of spark channels are ignited in the switch with electrical isolation between the channels and the characteristics of this switch are better. At a low triggering voltage pulse rise rate (less than 250 kV/ μ s), better characteristics are realized in the switch without electrical isolation between the channels.

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I. INTRODUCTION

Linear transformer drivers (LTDs) are under active development for high-voltage, high-current pulsed-power generators, and may significantly reduce their cost and size [1–5]. LTDs are based on the use of a primary capacitive storage unit with an energy output time of about 100 ns. The capacitive energy storage is divided into sections, each switched by its own gas spark switch. The number of switches can considerably exceed 10^4 in the newly developed petawatt-class LTDs [6–8]. The parameters of the primary energy storage device and LTD depend on the parameters of the switch, and studies of the different types of gas spark switch are therefore given special attention [9–14].

One avenue for the development of LTD generators is the use of atmospheric pressure air as insulation for the LTD stages and the working medium of the switches [15–17]. This requires increasing the length of the surface between the high-voltage and low-voltage electrodes of the switch, and for this, the planar geometry of the switch is used [16–19]. The interelectrode gap of the planar switch is divided into a series of connected small gaps using ball

electrodes, and parallel rows of these ball electrodes allow for multichannel switching. The important parameters of the switch, such as its resistance, inductance, dissipated energy and lifetime, are determined by the number of parallel ignited channels.

The switch and its triggering system should be considered together, as a single coupled system, when solving the multichannel switching problem. Obviously, the higher the amplitude and rise rate of the triggering voltage pulse, the better. However, insulation requirements are increasing and the technical implementation of the triggering system is becoming more complicated, especially for multisection installations. It is necessary to optimize the parameters of the triggering system that provide the multichannel switching mode, and optical diagnostic methods can be used to study multichannel switching and optimize these parameters [10,20,21].

This paper presents the results of a study of the probability of ignition of parallel spark channels in a multigap gas switch at atmospheric pressure under different operating conditions, utilizing an optical diagnostic system. We studied the influence of the rate of rise of the triggering voltage in the range of 100–800 kV/ μ s, the electrical decoupling between the channels and the auxiliary discharge of ionizing radiation on the number of channels. The dissipated energy of parallel spark channels was calculated based on experimental data on the number of channels. The calculation results allow us to reasonably choose the parameters of the triggering pulse and the design of the switch.

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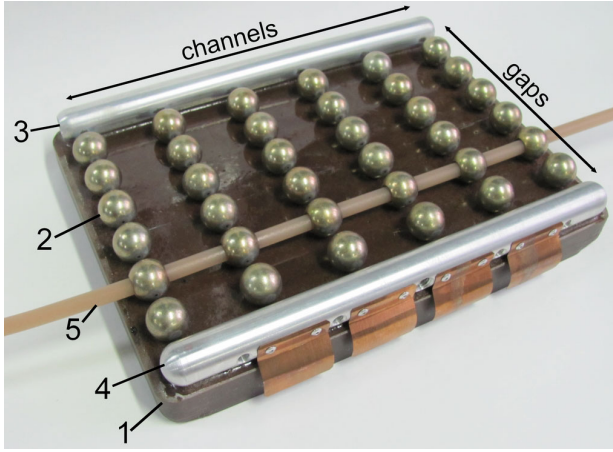


FIG. 1. Design of the switch with isolation between the channels: (1) epoxy slab; (2) intermediate ball electrodes; (3, 4) high- and low-voltage end electrodes; (5) triggering wire.

II. APPARATUS

A. Switch

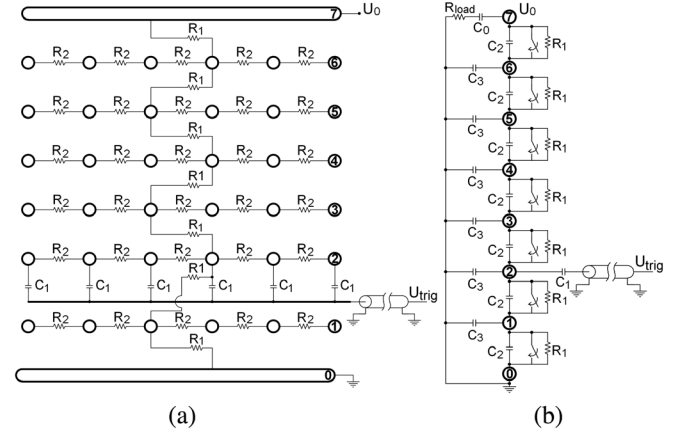
The design of the switch is shown in Fig. 1. The gap between the high-voltage (3) and low-voltage (4) electrodes is divided into seven serial gaps using intermediate electrodes (2). The high-voltage and low-voltage electrodes are cylinders with a diameter of 22 mm, while the intermediate electrodes are balls with the same diameter. The length of a single gap is 6 mm, giving a total gap for the switches of 42 mm. The ball electrodes are divided into six groups, forming six parallel channels. The switch electrodes are assembled on an epoxy slab (1).

The voltage across the gaps is distributed using a resistive voltage divider, in which the resistors are connected in series in one of the channels between the high- and low-voltage electrodes. Conducting rubber cords run in parallel to the high- and low-voltage electrodes inside the slab, ensuring that the voltage is distributed over the electrodes in all the other channels. The resistance of the rubber between adjacent channels is $\sim 0.8 \text{ M}\Omega$.

A triggering pulse is supplied to each of the channels to the electrodes of the third row, relative to the grounded side. These electrodes contain holes of diameter 9 mm, through which a triggering wire (5) with diameter of 3 mm passes with polyethylene insulation.

The dimensions of the switch are $298 \times 220 \times 50 \text{ mm}^3$.

An equivalent electrical scheme of the switch during charging of the capacitive storage device and an electrical scheme for a single switch channel at triggering are shown in Fig. 2. During charging, the voltage is distributed uniformly over the switch electrodes. At a charging voltage of 100 kV, the potential difference between the electrodes ($U_{\text{gap}} = U_0/7$) is less than 14.5 kV. The self-breakdown voltage of the gaps in air at atmospheric pressure is 18–19 kV.



$$U_{\text{trig},2} \sim U_{\text{trig}} \frac{C_1}{C_1 + C_3 + 2 \cdot C_2} \sim 0.41 \cdot U_{\text{trig}}. \quad (1)$$

The potential from a triggering pulse on adjacent electrodes is described by the following expressions [22]:

$$U_{\text{trig},3} = U_{\text{trig},2} \frac{\text{sh}(5 \cdot a)}{\text{sh}(6 \cdot a)} \approx 0.117 \cdot U_{\text{trig}} \quad (2)$$

$$U_{\text{trig},4} = U_{\text{trig},2} \frac{\text{sh}(4 \cdot a)}{\text{sh}(6 \cdot a)} \approx 0.033 \cdot U_{\text{trig}} \quad (3)$$

$$U_{\text{trig},5} = U_{\text{trig},2} \frac{\text{sh}(3 \cdot a)}{\text{sh}(6 \cdot a)} \approx 0.009 \cdot U_{\text{trig}} \quad (4)$$

$$U_{\text{trig},6} = U_{\text{trig},2} \frac{\text{sh}(2 \cdot a)}{\text{sh}(6 \cdot a)} \approx 0.003 \cdot U_{\text{trig}} \quad (5)$$

$$U_{\text{trig},1} = U_{\text{trig},2} \frac{\text{sh}(1 \cdot a)}{\text{sh}(2 \cdot a)} \approx 0.108 \cdot U_{\text{trig}}, \quad (6)$$

where $a = \ln[1 + \frac{C_1}{2 \cdot C_2} \cdot (1 + \sqrt{\frac{4 \cdot C_2}{C_1} + 1})]$.

The voltage in the gaps on different sides of triggering electrode 2 is not the same. The voltage in the gaps between electrodes 2 and 3 and electrodes 1 and 2, taking into account the initial distribution of the charging voltage (U_0), is the following:

$$\begin{aligned} U_3 - U_2 &= \frac{U_0}{7} + (U_{\text{trig},3} - U_{\text{trig},2}) \\ &\approx U_0/7 - 0.293 \cdot U_{\text{trig}}, \end{aligned} \quad (7)$$

$$\begin{aligned} U_2 - U_1 &= \frac{U_0}{7} + (U_{\text{trig},2} - U_{\text{trig},1}) \\ &\approx U_0/7 + 0.302 \cdot U_{\text{trig}}. \end{aligned} \quad (8)$$

A higher voltage is generated in the gap between electrodes 2 and 3 according to expressions (7) and (8) and taking into account the different polarity of the charging voltage (U_0) and the triggering voltage (U_{trig}) (time t_1). The voltage in this gap increases by a factor of more than 2.5, which leads to the breakdown of this gap. After breakdown of the gap between electrodes 2 and 3, a triggering voltage is applied to electrode 3 (time t_2), and breakdown of the gap between electrodes 3 and 4 occurs, and so on (time $t_3 - t_5$). After breakdown of the gaps between electrodes 2 and 7, the capacitive storage voltage is applied to the gaps between electrodes 0 and 1 and electrodes 1 and 2 (time t_6). Breakdown of the last gaps can occur when the voltage is more than 4 times higher than the initial value. It can be seen that as the gaps are broken down, the possible overvoltage at the unbroken gaps increases.

The number of parallel spark channels in the gaps cannot exceed the number of channels in the gap, which breaks first (the gap between electrodes 2 and 3), since the electrodes of one row are electrically isolated (R_2 is very high) and the discharge current cannot be redistributed between them. The maximum possible number of parallel spark channels in the gap is equal to the number of ball electrodes in the row, i.e., six. The actual number of channels is determined by the rate of increase in the triggering voltage pulse.

However, if the electrodes of one row are electrically connected ($R_2 \approx 0$), then the discharge current can be redistributed between the electrodes of the same row, and a different number of channels can be ignited in the gaps. We expect an increase in the number of parallel channels with the successive breakdown of gaps due to an increase in overvoltage. To verify this, changes were made to the design of the multichannel multigap switch.

The design of the modified switch is shown in Fig. 4. We removed the electrical isolation between the channels in this version. Ball electrodes in one row are connected by stainless steel rods with a diameter of 6 mm [thus $R_2 = 0$ in Fig. 2(a)]. The design of the switch allowed us to install serrated stainless steel blades on the rods, as shown in Fig. 4. These blades are intended to give ignition of the corona discharge when the capacitive storage device is charged. The thickness of the blades was 0.2 mm, and their length was selected to give corona discharge ignition at the blade at low voltage and to ensure that triggering breakdown did not occur from the blade but from a ball electrode. The corona discharge current was $\sim 1 \mu\text{A}$ at a switch voltage of about 70 kV, increasing to $\sim 100 \mu\text{A}$ as the voltage increased to 100 kV.

The triggering system remained the same, and the triggering pulse was supplied through separation capacitances to each electrode in the third row, relative

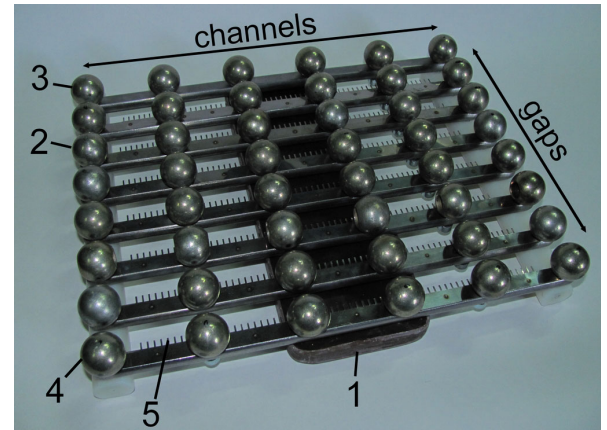


FIG. 4. Design of the switch without isolation between the channels: (1) resistive voltage divider inside epoxy slab; (2) intermediate ball electrodes; (3, 4) high- and low-voltage end electrodes; (5) corona discharge blades.

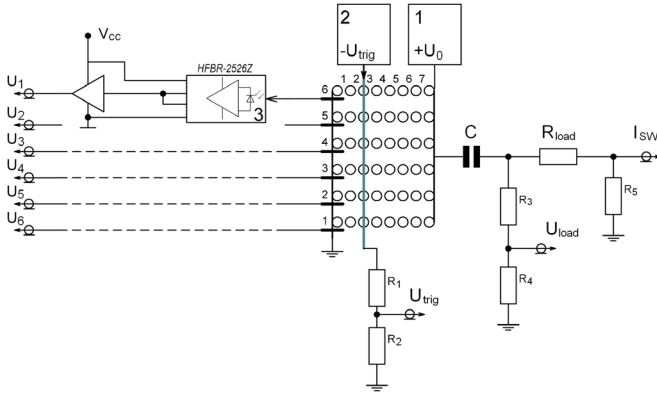


FIG. 5. Scheme of the test bed for switch testing: (1) HV power supply; (2) triggering generator; (3) photodiode and preamplifier circuit.

to the grounded side. The dimensions of the switch were unchanged.

B. Switch-testing apparatus

A scheme for a test bed for the switch tests is shown in Fig. 5. A capacitive energy storage device $C = 20$ nF (two series-connected capacitors from General Atomics GA35426, 100 kV, 40 nF) is charged with a positive polarity voltage of up to 100 kV from an high voltage (HV) power supply (1). The switch is triggered by a negative polarity voltage pulse from a triggering generator (2). Three triggering pulse generators with voltage rise rates of 100, 250 and 800 kV/ μ s were used (see Fig. 6). After switch triggering, the capacitive storage is discharged via a load $R_{load} = 3.8 \Omega$.

The triggering voltage $U_{trig}(t)$ is monitored using the resistive divider R_1-R_2 ; the load voltage $U_{load}(t)$ is monitored through the resistive divider R_3-R_4 ; and the switch current $I_{SW}(t)$ is monitored through the resistive shunt R_5 . Figure 7 shows an example of current waveforms when using the switch without electrical isolation between channels for three cases with different triggering voltage rise rates. A decrease in the amplitude and an increase in the

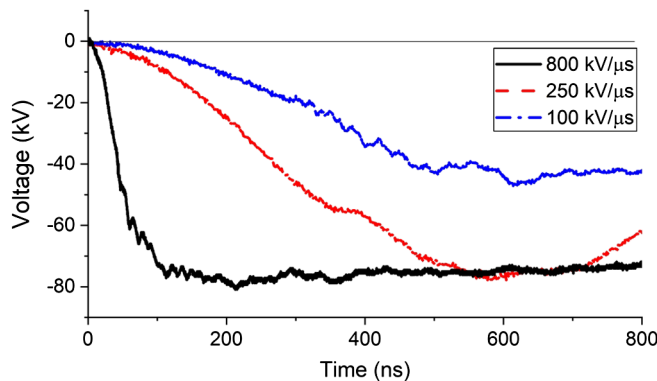


FIG. 6. Triggering pulse waveforms.

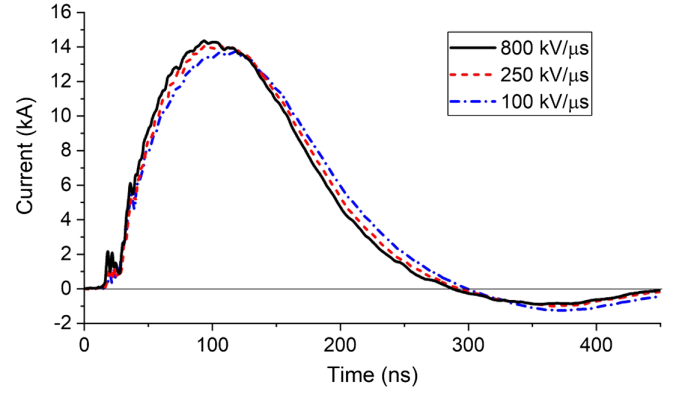


FIG. 7. Switch current waveforms.

current pulse front with a decrease in the triggering pulse rise rate is associated with a decrease in the number of parallel channels.

An optical system is used to determine the number of channels in the switch gaps. The system consists of six collimators with an extended hole and the light is fed through a fiber to a photodiode with a preamplifier circuit (HFBR-25X6Z, Avago Technologies). Six signals $U_1 - U_6$ from each photodiode are fed into an amplifier and then recorded using Tektronix TDS 3054B digital oscilloscopes with a bandwidth of 500 MHz (see Fig. 5). The time resolution of the photodiodes and amplification circuit is a few nanoseconds.

The arrangement of the collimators in the switch is shown in Fig. 8. Six collimators were arranged in a row in one of seven positions. Each position corresponds to one of the seven gaps of the switch. The dimensions and arrangement of the collimators are adjusted to exclude light from neighboring gaps, i.e., each collimator only registers light from the gap over which it is placed.

The research method is as follows. Six collimators were placed above gap 1 (see Fig. 8, side view). A series of

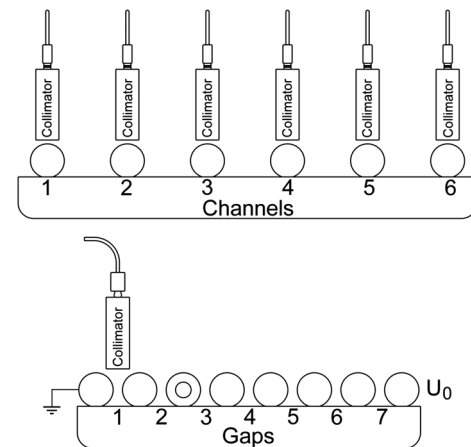


FIG. 8. Front and side views of the switch and arrangement of the collimators.

$N_0 = 50$ successive pulses was performed. For each pulse, the signals from the photodiodes were recorded, which made it possible to determine how many and which channels were ignited in gap 1. The number of channel ignition cases N and the probability of ignition $(\frac{N}{N_0}) \cdot 100\%$ were calculated for each of the six channels in gap 1. In this calculation, only cases of channel ignition during the front of the discharge current pulse were taken into account. Six collimators were then moved to position 2 above gap 2. A series of 50 successive pulses was performed again. The number of channel ignition cases and the probability of ignition were calculated for each of the six channels in gap 2. Six collimators were then moved to position 3 above gap 3 and so on. Thus, we sequentially placed the collimators in seven positions and performed 50 pulses for each of them. The full series for calculating the probability of ignition of each of the six channels in each of the seven gaps was 350 pulses under fixed operating conditions.

In addition, the statistics for the delay time between the triggering pulse and the breakdown of the switch were collected using a series of 350 pulses. The delay time was determined as the time between the 10% levels of the amplitude of the triggering pulse and the load voltage. The statistical delay time was characterized by the average delay time and the standard deviation (jitter of the switch).

Examples of signals from the sensors are given in Fig. 9. In the first example, all six channels are ignited in a gap with a spread of 10 ns, while in the second, five of the six

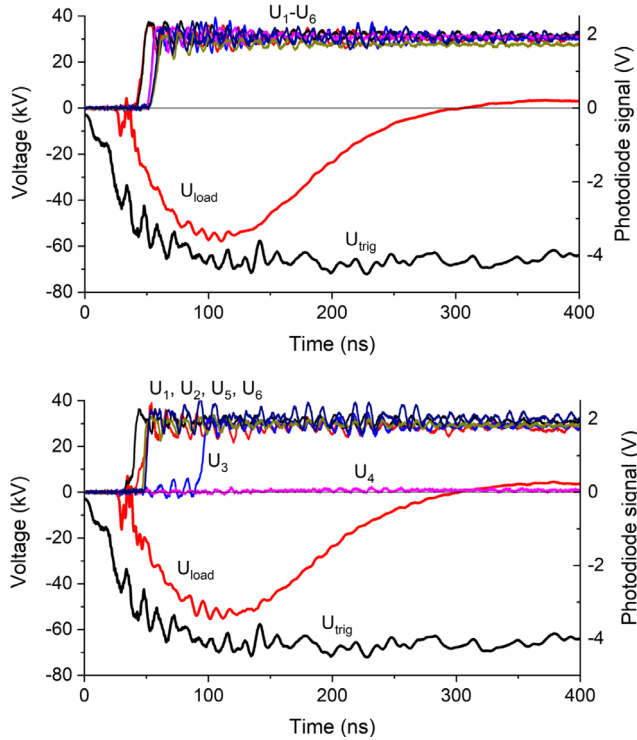


FIG. 9. Triggering pulse waveform U_{trig} , load voltage waveform U_{load} and signals from six photodiodes $U_1 - U_6$.

channels are ignited, and the third channel is ignited with a delay of 50 ns relative to the remaining channels.

III. RESULTS

Figure 10 shows the probabilities of ignition of channels in each of the seven gaps of the switch with electrical isolation between the channels. The results show that the number of channels in all the gaps is approximately the same in the switch with electrical isolation between the channels, and that this is determined by the number of channels initiated by the triggering pulse in gap 3, which breaks first. A rise rate of the triggering pulse of $\sim 800 \text{ kV}/\mu\text{s}$ provides the ignition of four parallel channels in all gaps with a probability of at least 85%. The number of channels decreases with a decrease in the rise rate of the triggering pulse, and the probability of ignition of four parallel channels in the gaps does not exceed 32% with a threefold decrease in the rise rate of the triggering pulse.

The situation changes when there is no electrical isolation between the channels. Figure 11 shows the

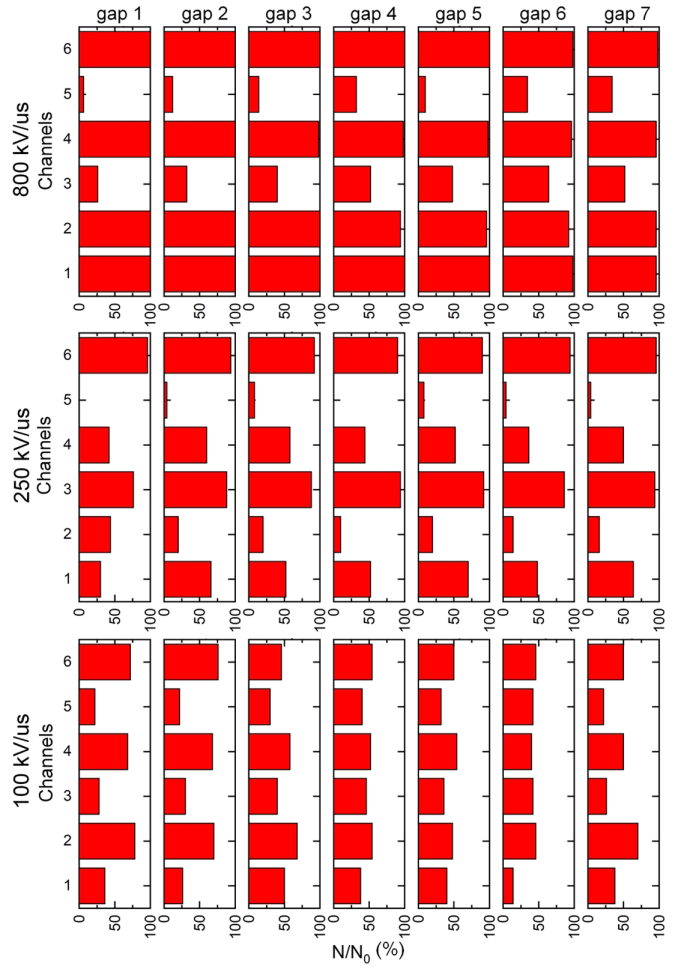


FIG. 10. Probability of ignition of spark channels in the gaps of the switch with electrical isolation between the channels, for rise rates of the triggering pulse of 800, 250 and 100 kV/ μs .

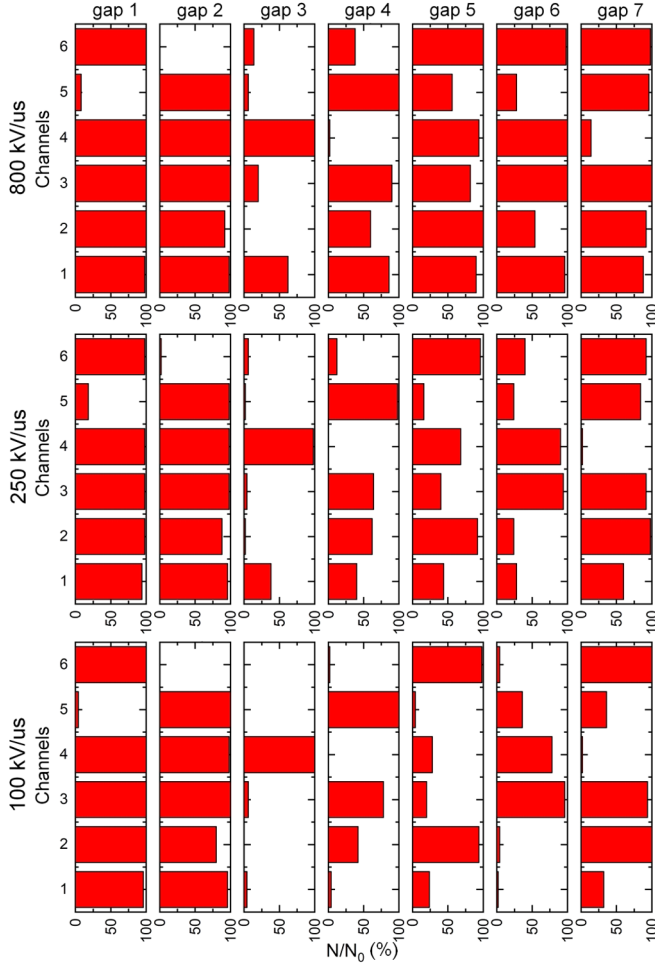


FIG. 11. Probability of ignition of spark channels in the gaps of the switch without electrical isolation between the channels, for rise rates of the triggering pulse of 800, 250 and 100 kV/μs.

probabilities of ignition of the channels in each of the seven gaps of the switch without electrical isolation between the channels. Only one channel is mainly ignited in the triggering gap 3. The number of parallel channels increases with the breakdown of subsequent gaps, due to an increase in overvoltage. The largest number of channels is realized in the gaps breaking through last: the gap closest to the capacitive storage (gap 7) and the two gaps at the side of the grounded electrode (gaps 1 and 2). The number of channels decreases with a decrease in the rise rate of the triggering voltage, as expected; however, five channels are ignited in gaps 1 and 2, and four channels are ignited in gap 7, with a probability of more than 75% even at a rise rate of 100 kV/μs.

The additional blade electrodes of the auxiliary corona discharge did not affect the number of channels ignited, although the auxiliary discharge affected the jitter of the switch. Table I shows data on the jitter of the switch for various configurations, depending on the rise rate of the triggering pulse. The stabilizing effect of the corona

TABLE I. Switch jitter, calculated using a series of 350 pulses.

$\frac{dU_{\text{trig}}(t)}{dt}$, kV/μs	Jitter, ns		
	Switch with electrical isolation between the channels	Switch without electrical isolation between the channels and without auxiliary corona discharge	Switch without electrical isolation between the channels and with auxiliary corona discharge
800	1.29	2.54	1.11
250	32.80	26.09	8.22
100	62.52	52.59	13.26

discharge is observed to be significant when trigger pulses with a low rise rate are used. Corona discharge reduces jitter by a factor of 3–4 at a trigger pulse rise rate of below 250 kV/μs. For a high rise rate of the triggering pulse (~800 kV/μs), the effect of the corona discharge is less pronounced.

IV. DISCUSSION

Experimental data on the number of channels make it possible to compare the level of energy loss in the switch in the presence and absence of electrical isolation between the channels. Dissipated energy in the spark channels of a seven-gap switch can be written as

$$E_{\text{sw}}(t) = \sum_{i=1}^7 E_i(t), \quad (9)$$

where $E_i(t)$ is the dissipated energy of the system of parallel spark channels in gap i . In the calculations, we assumed a uniform distribution of current between parallel channels of the same gap, i.e., the current through a single channel in the gap is

$$I_i(t) = I_{\text{sw}}(t)/N_i, \quad (10)$$

where $I_{\text{sw}}(t)$ is the switch current and N_i is the number of spark channels in gap i .

With a 1–10 kA spark channel current and submicro-second pulse duration, satisfactory agreement with the experiment is provided by the Braginskii model (hydrodynamic expansion of a spark channel in an approximation of constant conductivity) [23]. The model gives an expression for the radius of the expanding channel with current $I_i(t)$:

$$r_i(t) = r(0) + \left(\frac{4}{\rho_0 \pi^2 \xi \sigma} \right)^{1/6} \left(\int_0^t |I_i(t)|^{2/3} dt \right)^{1/2}, \quad (11)$$

where $r(0) \sim 0.05$ mm and is the initial channel radius, ρ_0 is the gas density at which the discharge occurs,

TABLE II. Number of parallel channels with a probability of ignition of more than 90% and the energy dissipated in the switch at different rise rates of the triggering pulse.

$\frac{dU_{\text{trig}}(t)}{dt}$, kV/ μ s	N_1	N_2	N_3	N_4	N_5	N_6	N_7	E_{sw} , J
Switch with electrical isolation between the channels								
800	4	4	4	4	4	3	3	13.34
250	1	1	1	1	1	1	2	21.76
100	1	1	1	1	1	1	1	22.54
Switch without electrical isolation between the channels								
800	5	5	1	2	3	4	4	14.75
250	5	4	1	1	1	2	2	18.01
100	5	4	1	1	2	1	2	18.60

σ is the specific electrical conductivity and ξ is a dimensionless constant. For air under normal conditions, $\rho_0 = 1.2 \times 10^{-3}$ g/cm³, $\xi \approx 4.5$ and $\sigma = 300$ ($\Omega \cdot \text{cm}$)⁻¹ [24]. Using (11) and experimental current waveforms, we can calculate the resistance and dissipated energy of a system of N_i parallel spark channels in each of the seven gaps.

The resistance of parallel spark channels in a single gap is

$$R_i(t) = \frac{1}{N_i} \cdot \frac{l}{\pi r_i(t)^2 \sigma}. \quad (12)$$

The energy dissipated in a single gap is

$$E_i(t) = \int_0^t I_{\text{sw}}(t)^2 R_i(t) \cdot dt \quad (13)$$

Table II shows the data on the number of parallel channels in the gaps of the switch. The number of channels ignited with a probability of more than 90% is taken as the number of spark channels. Table II also shows the energy dissipated in the switch, calculated using Eqs. (9)–(13). At a triggering pulse rise rate of ~ 800 kV/ μ s, the dissipated energy is ~ 13.3 J for the switch with electrical isolation between channels and ~ 14.7 J for the switch without electrical isolation between channels. With a decrease in the rise rate of the triggering pulse from 800 to 100 kV/ μ s, the loss of switching energy increases by a factor of 1.7 for the switch with electrical isolation between channels, and less than 1.3 for the switch without electrical isolation. The energy dissipated in the switch without electrical isolation between channels becomes less than in the switch with electrical isolation at a low triggering pulse rise rate (100–250 kV/ μ s).

V. SUMMARY

The number of channels and their distribution over consecutive gaps depends on the electrical isolation between the channels. If there is electrical isolation, the

number of channels in all the gaps is approximately the same, and is determined by the number of channels initiated in the triggering gap. A rise rate for the triggering pulse of about 800 kV/ μ s provides the ignition of four parallel channels in all gaps with a probability of at least 85%. The number of channels decreases with a decrease in the rise rate of the triggering pulse. Hence, the probability of ignition of four parallel channels in the gaps does not exceed 32% with a threefold decrease in the rise rate.

If there is no electrical isolation, only one channel is mainly ignited in the triggering gap, although the number of parallel channels increases with the successive breakdown of gaps. The largest number of channels is realized in the gaps breaking through last. Four or five channels are ignited in these gaps with a probability of more than 75%, even for a rise rate of the triggering pulse of 100 kV/ μ s. The energy dissipated in this switch is less than in the switch with electrical isolation between the channels at a triggering pulse rise rate of 100–250 kV/ μ s. Thus, the switch without isolation between the channels has an advantage when a trigger pulse with a low rise rate is used.

ACKNOWLEDGMENTS

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