

SYNTHESIS OF THE MULTIPOLE LENS POLE SHAPE FROM CONJUGATED STRAIGHT LINES AND ARCS

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Abstract

The calculation technique for multipole design is described for the case when the pole shape is consisted of different areas. Some requirements can be imposed on the curvature of these areas. The pole shape of the dipole magnets, quadrupoles and sextupoles for the 2 GeV accelerator - synchrotron storage ring complex developing in KIPT were designed using the described technique of calculation.

1 INTRODUCTION

Reaching of required parameters of modern installations [1,2] has demanded of magnets with complex multipolar composition of the field. The necessity of modelling of such complex fields (stipulated by demanded allowable deviations $\sim 10^4$) generates desire to have expression connecting a field and geometric performances of a magnet, namely with the form of a pole. Even the saturation of iron can be compensated by preliminary geometric distortions of a pole shape [3].

As is known, it is possible to express field both through the complex potential $z(\omega)$, and through the inverse function to the complex potential, $\omega(z)$ ($\omega(z)$ - conformal map of the band $0 \leq \text{Im}(z) \leq H$ on a pole [4]).

$$B = -i\overline{(dz/d\omega)} = -i\overline{(d\omega/dz)} \quad (1)$$

Following exposition is devoted to deriving of the map of the line band $0 \leq \text{Im}(z) \leq H$ on the band of pole area, $\omega = x + iy$.

2 THE "BAND TO BAND" CONFORMAL MAPPING

Let's consider a conformal map of a line band $0 \leq \text{Im}(z) \leq H$ of an area $z = t + ih$ on a band of a pole area $\omega = x + iy$ (Fig.1). Let the angle of declination $v = v(t)$ of a tangent to L in a point ω that is appropriate to point t is known in each point t of boundaries of a band $0 \leq \text{Im}(z) \leq H$. Let also $dz = dt$ and $d\omega = |d\omega| \exp[iv(t)]$ are elements of a boundary of a band and contour L , appropriate one another in considered conformal mapping, then

$$d\omega/dz = \exp[iv(t)] \cdot |d\omega|/dt \quad (2)$$

Let's remark that:

$$-i\ln[d\omega/dz] = v(t) - i\ln[|d\omega|/dt] = g(z), \quad (3)$$

where $g(z)$ - function, which real part on boundaries of a band accepts significances $v(t)$. Obviously, that a deriving map has a form:

$$\omega(z) = C \int_{z_0}^z \exp[ig(z)] dz + C_0; \quad (4)$$

where C, C_0 are constants of an integration.

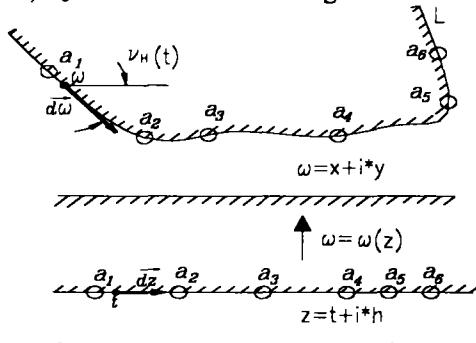


Fig.1 Map of a band $0 \leq \text{Im}(z) \leq H$ on a band with any boundaries.

Let's establish the correspondence $\omega(0) = 0$; that is $C_0 = 0$. For $\omega(z)$, the ratio of real and imaginary parts is important. Therefore let's assume $C = 1$. The function $g(z)$, by virtue of an above-stated property (3), is restored by an integral of the Schwarz for a band. For map of a circle to any simply connected region the formula of a kind (4) is known as the formula Chizotii [4].

2.1 Integral of the Schwarz for a band

The integral of the Schwarz for a circle $|\zeta| \leq 1$ has a form

$$G(\zeta) = \frac{1}{2\pi} \int_{-\pi}^{\pi} V(\exp(i\tau)) \frac{\exp(i\tau) + \zeta}{\exp(i\tau) - \zeta} d\tau; \quad (5)$$

where τ is an angular coordinate of a plane ζ containing a circle $|\zeta| \leq 1$. Let's consider a conformal mapping of a band $0 \leq \text{Im}(z) \leq H$ of a plane $z = t + ih$ on a circle $|\zeta| \leq 1$ of a plane $\zeta = r \cdot \exp(it)$,

$$\zeta(z) = \text{th}(\pi(2z - iH)/4H), \quad (6)$$

transferring the lower and upper boundaries of a band in the lower and upper semicircles accordingly, also we shall designate $G[\zeta(z)] = g(z)$, $V[\exp(it)] = v(t)$. By allocating two intervals of an integration, $\tau \in [-\pi, 0] \Rightarrow t \in [-\infty, \infty]$; $\tau \in [0, \pi] \Rightarrow t \in [\infty, -\infty]$ and, by making a change of variables, we shall receive

$$g(z) = \frac{i}{2H} \left\{ - \int_{-\infty}^{\infty} v_0(t) \left[\text{cth} \frac{\pi(t-z)}{2H} - \text{th} \frac{\pi t}{H} \right] dt + \right.$$

$$\int_{-\infty}^{\infty} v_H(t) \left[\operatorname{th} \frac{\pi(t-z)}{2H} - \operatorname{th} \frac{\pi t}{H} \right] dt. \quad (7)$$

The first integral responses for degrees of a symmetry, the second - for the form of a pole. The preservation of an addend $\operatorname{th}(\pi t/H)$ under the integral (in [4] it is brought in constants of an integration) allows, by substituting (7) in (4) to receive analytical expression for map "band to band". The formulas (4,7) allow to describe practically all "Halbach geometries" [5].

3 INFLUENCE OF VARIOUS AREAS OF THE STRUCTURE ON THE FIELD

The formulas (4,7) result in expression for a conformal mapping "band to band".

$$\omega(z) = \int_{z_0}^z \exp[G(z)] dz; \quad (8)$$

where

$$G(z) = \frac{1}{2H} \int_{-\infty}^{\infty} v_0(t) \left[\operatorname{cth} \frac{\pi(t-z)}{2H} - \operatorname{th} \frac{\pi t}{H} \right] dt - \frac{1}{2H} \int_{-\infty}^{\infty} v_H(t) \left[\operatorname{th} \frac{\pi(t-z)}{2H} - \operatorname{th} \frac{\pi t}{H} \right] dt \quad (9)$$

We shall define the function describing the behaviour of an angle of declination of a structure of the pole $v_H(t)$, as

$$v_H(t) = \begin{cases} \operatorname{const} = U_{-\infty}, & t \in [-\infty, a_1] \\ q_j(t), & t \in [a_j, a_{j+1}] \quad j = 1 \Lambda M-1; \\ \operatorname{const} = U_{\infty}, & t \in [a_1, \infty] \end{cases} \quad (10)$$

M , is number of points on the upper coast of a band, between which $v_H(t)$ is continuous. In case of a multipolar symmetry, $v_0(t)$ is determined as:

$$v_0(t) = \begin{cases} \operatorname{const} = U_{\text{mult}}, & t \in [-\infty, 0] \\ \operatorname{const} = 0, & t \in [0, \infty] \end{cases} \quad (11)$$

For a dipole symmetry $U_{\text{mult}}=0$; for a quadrupole symmetry $U_{\text{mult}}=-\pi/2$; for sextupole $U_{\text{mult}}=-\pi/3$; etc.

We shall rewrite (8) under of accepted definition of the angle of declination of a pole structure (10) as:

$$\omega(z) = \int_{z_0}^z \exp \left[G_{\text{mult}}(z) + G_{le}(z) + G_{re}(z) + \sum_{j=1}^{M-1} G_j(z) \right] dz; \quad (12)$$

where

$$\exp[G_{\text{mult}}(z)] = \left[1 - \exp(-\pi z/H) / \sqrt{2} \right]^{U_{\text{mult}} / \pi}; \quad (13)$$

This factor originating from the first integral of the formula (9) describes influence of the degree of the symmetry on the field. So for the dipole symmetry $\exp[G_{\text{mult}}(z)]=1$.

$$G_{le}(z) = \frac{U_{-\infty} z}{2H} - \frac{U_{-\infty}}{\pi} \left(\ln \sqrt{2} + \ln \frac{\operatorname{ch}(\pi(a_1-z)/2H)}{\operatorname{ch}(\pi a_1/H)} \right) \quad (14)$$

This member responses for the left-hand edge of a pole.

$$G_{re}(z) = \frac{U_{-\infty} z}{2H} + \frac{U_{-\infty}}{\pi} \left(\ln \sqrt{2} + \ln \frac{\operatorname{ch}(\pi(a_2-z)/2H)}{\operatorname{ch}(\pi a_2/H)} \right) \quad (15)$$

This member responses for the right-hand edge of a pole. $G_{le}(z)$, $G_{re}(z)$ is an outcomes of an integration of the second integral of expression (9) in limits $[-\infty, a_1]$, $[a_2, \infty]$ accordingly.

$$G_j(z) = -\frac{1}{2H} \int_{a_j}^{a_{j+1}} q_j(t) \left[\operatorname{th} \frac{\pi(t-z)}{2H} - \operatorname{th} \frac{\pi t}{H} \right] dt \quad (16)$$

This member responses for a area of a pole between points a_j , a_{j+1} .

Formally, each of the members $G_{le}(z)$, $G_{re}(z)$, $G_j(z)$ can be considered as function generating a conformal mappings of a rectilinear band on a band which at upper boundary is tangent to the lower one everywhere, except the area described by the appropriate member. Let's a pole of a dipole magnet is determine by a specific behaviour of an angle of declination of a structure of a pole between 6 points in Fig.2. To each of areas between points $-\infty, a_1, a_2, a_3, a_4, a_5, a_6, \infty$ we shall get in accordance with the conformal mapping.

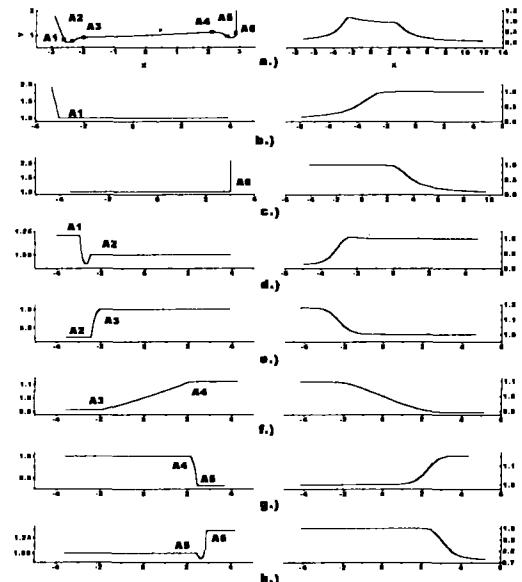


Fig.2 Influence of areas of the pole structure to the field. At the left there are area of a pole structure. On the right fields, appropriate to these areas of a pole structure.

For example, we shall consider the contribution for a left-hand slope of a pole $(-\infty, a_1)$. Let angle of declination forming of a pole structure $v_H(t)$ (10) is determined in such a manner that: $(q_j(t)=0, j=1, M, U_{\infty}=0)$. Then the expression (12) acquires a form

$$\omega(z) = \int_{z_0}^z \exp[G_{le}(z)] dz; \quad (17)$$

It is a conformal mapping of a rectilinear band on a band, which the lower boundary is a direct line, upper: an angle between direct lines is tangent to axes OX, the other one intersect the first line under the angle U_{∞} in a point A_1 , Fig.2.b. Similarly it is possible to construct maps, therefore are fields for each site of a pole structure. Fig.2 illustrates the contribution separate site of a pole structure between points a_j in a field for a dipole magnet.

The influence of a different areas of a structure on a field consists of the following: *the field, in coordinates of a plane containing a rectilinear band, is equal to the product of fields from elementary conformal mappings, which are determined by the initial parameters of the areas.*

4 THE MULTIPOLAR ANALYSIS OF A FIELD

Using expression (1), (9), we shall derive an expression for the field in coordinates of the band $0 \leq \text{Im}(z) \leq H$

For the dipole symmetry $v_0(t)=0$

$$B(z) = \exp[-F(z)] \quad (18)$$

where

$$F(z) = -\frac{1}{2H} \int_{-\infty}^{\infty} v_H(t) \left[t \operatorname{th} \frac{\pi(t-z)}{2H} - \operatorname{th} \frac{\pi}{H} \right] dt \quad (19)$$

as

$$d\omega(z) = \exp[F(z)] dz$$

that

$$\frac{d^i B(z)}{d\omega(z)^i} = \exp[-F(z)] \frac{d}{dz} \left[\frac{d^{i-1} B(z)}{d\omega(z)^{i-1}} \right]. \quad (20)$$

By applying this procedure so many times as many derivatives on the field we know, we shall get a system, which can be solved concerning a derivatives of function $F(z)$. And, as we are free to establish the correspondence $\omega(0)=0$:

$$\begin{cases} B(0) = \exp[-F(0)] \\ B'(0) = -F'(0)B(0)^2; \\ B''(0) = (2F'(z)^2 - F''(z))B(0)^3; \\ B^{(3)}(0) = (-6F'(0)^3 + 7F'(0)F''(0) - F^{(3)}(0))B(0)^4 \end{cases} \quad (21)$$

For the quadrupole symmetry

$$v_0(t) = \begin{cases} -0.5\pi, & t \in [-\infty, 0] \\ 0, & t \in [0, \infty] \end{cases} \quad (22)$$

$$d\omega(z) = \sqrt{2/[1 - \exp(-\pi z/H)]} \exp[F(z)] dz \quad (23)$$

$$B(z) = \sqrt{[1 - \exp(-\pi z/H)]/\sqrt{2}} \exp[-F(z)] \quad (24)$$

$$\frac{d^i B(z)}{d\omega(z)^i} = \frac{\sqrt{[1 - \exp(-\pi z/H)]/\sqrt{2}}}{\exp[F(z)]} \frac{d}{dz} \left[\frac{d^{i-1} B(z)}{d\omega(z)^{i-1}} \right] \quad (25)$$

$$\begin{cases} B'(0) = \frac{\pi}{H^2 \sqrt{2} \exp[2F(0)]}; \\ B^{(3)}(0) = \frac{-\pi^2(\pi + 4HF'(0))}{H^3 8 \exp[4F(0)]}; \\ B^{(5)}(0) = \frac{\pi^3(2\pi^2 + 13H\pi F'(0) + 26H^2 F'(0)^2 - 9H^2 F''(0)^2)}{H^5 8 \sqrt{2} \exp[6F(0)]}; \\ K \end{cases} \quad (26)$$

All the even derivatives are equal to zero at the point $\omega=0$. The influence of the multipolar member (13) consists of that. The analysis of expressions (26) shows, that if $v_H(t) + \pi/4$ is the odd function (the right member of a pole is symmetric left-hand), the only derivatives allowed for a quadrupole symmetry, with numbers $n = 1 + 4*i$ are not equal to zero. Using the determined with the help of (26) the value of the derivatives of $F(z)$, one can restored the function $F(z)$ itself, and the inverse to the complex potential function as well. Thus, knowing a field it is possible to restore the pole structure which will realize this field.

5 CONCLUSION

The above mentioned expressions allow to calculate the field and the forms of poles of multipoles if the function of an angle of declination forming of a pole structure $v_H(t)$ - in coordinates of a rectilinear band $0 \leq \text{Im}(z) \leq H$ is known. The inverse solution is possible to get as well: by a field is discovered $v_H(t)$, so also form of a pole. The form of function $v_H(t)$ can be those, that of a pole will take the form necessary of technological reasons. These circumstances have allowed to develop the program of synthesis of a pole structure. Input data of the program are: the field specified explicitly or as series, and some design data of a pole. The Fig.2 is plotted using this program.

6 REFERENCES

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